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# Some Operational Formulations For Computational Solutions Of Underwater Acoustic Scattering Problems

Environmental and Tactical Support Systems Department



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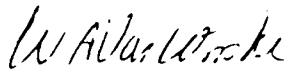
**Naval Underwater Systems Center**  
Newport, Rhode Island/New London, Connecticut

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## **Preface**

This document was prepared for the Office of the Associate Technical Director for Technology by Dr. David Middleton.

**Reviewed and Approved: 21 November 1989**

A handwritten signature in cursive script, appearing to read "W. A. Von Winkle".

**W. A. Von Winkle**

**Head, Environmental and Tactical Support Systems Department**

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<p>Scattering from ocean wave surfaces, volumes, and bottoms remains a perennial problem not only in underwater acoustics but also in the use of acoustical methods in remote sensing and modeling of the medium itself. Although analytic solutions are sometimes available, cf. [1], [6], in many important cases, particularly those involving multiple scatter and non-isogradian (<math>\nabla c \neq 0</math>) phenomena including the rôle of both stationary and moving arrays, and general geometries, effective modeling and quantitative, predictive results ultimately require computational methods. This is true for both deterministic and random media.</p> <p>It is the aim of this introductory study to present a combined analytical-operational framework from which computational solutions to underwater acoustic scattering problems, including relevant ocean boundary interactions, can be initiated and carried out. It is emphasized that here explicit computational procedures are <i>not</i> developed. Rather, the specific aim is to present</p>					
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the "macro-algorithms" from and to which appropriate software may be designed and applied. This is done by providing formal operational structures (with some special cases in which analytic solutions are obtainable). A collateral aim of this work is to entice interest in pursuing computational formulations, based on the various formal operational "solutions" derived here for both deterministic and general random acoustical (i.e., scalar) fields,  $\alpha(R,t)$ .

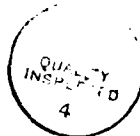
For inhomogeneous deterministic media ( $\nabla c \neq 0$ ;  $c = c(r,t) = c_0 + \alpha(r,t)$ , with  $\hat{c}$  nonrandom, for example), operational solutions may be derived directly: all representations of the medium (and boundaries) are equivalent. The resulting solutions provide a possible alternative approach to the current "standard" methods involving partial or parabolic equations (PE) developments [7], [8], at the same time including general arrays, geometries, and signals.

On the other hand, most of the scattering mechanisms in the ocean are essentially random. Accordingly, in these cases, scattering "solutions" are based on the appropriate Langevin equation governing propagation, namely, on the ensemble of representations  $\{\alpha(R,t)\}$  for which various appropriate probability measures (often nongaussian) are developed, based on both the physics, geometry, and the random mechanisms involved. Thus, practical solutions here are the various moments  $\langle \alpha \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$ , etc., and pdf's  $w_1(\alpha)$ ,  $w_1(\alpha_1, \alpha_2)$ , etc., which are needed, for example, in the calculation of scattering cross sections and subsequent signal processing for target detection and remote sensing [2]-[4].

The desired framework is obtained by recognizing that both the deterministic and random scattered fields in these linear media are representable as four-dimensional feedback systems, with the inhomogeneous portions (including the ocean interfaces) constituting the feedback operations. New features of this work include a combination of diagram methods, perturbational operational series, and equivalent (i.e., deterministic) media operators, which then provide the needed structure for both the direct and moment solutions  $\alpha$ , or  $\langle \alpha_1 \rangle$ , etc., independently, with the latter based on the resultant Dyson and Bethe-Salpeter forms, for  $\langle \alpha \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$ , etc. [2], [3]. Various analytical, iterative, and approximative examples and procedures are briefly presented, to illustrate the desired formal solutions and to provide elements of a framework for computational implementation.

The interfacing between these formally analytic solutions, their software realizations, and the acquisition of (nearly) on-line numerical results remain a major challenge.

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# Some Operational Formulations for Computational Solutions of Underwater Acoustic Scattering Problems\*

by

David Middleton\*\*

## Abstract

Scattering from ocean wave surfaces, volumes, and bottoms remains a perennial problem not only in underwater acoustics but also in the use of acoustical methods in remote sensing and modeling of the medium itself. Although analytic solutions are sometimes available, cf. [1], [6], in many important cases, particularly those involving multiple scatter and non-isogradian ( $\nabla c \neq 0$ ) phenomena including the rôle of both stationary and moving arrays, and general geometries, effective modeling and quantitative, predictive results ultimately require computational methods. This is true for both deterministic and random media.

It is the aim of this introductory study to present a combined analytical-operational framework from which computational solutions to underwater acoustic scattering problems, including relevant ocean boundary interactions, can be initiated and carried out. It is emphasized that here explicit computational procedures are *not* developed. Rather, the specific aim is to present the "macro-algorithms" from and to which appropriate software may be designed and applied. This is done by providing formal operational structures (with some special cases in which analytic solutions are obtainable). A collateral aim of this work is to entice interest in pursuing computational formulations, based on the various formal operational "solutions" derived here for both deterministic and general random acoustical (i.e., scalar) fields,  $\alpha(\mathbf{R}, t)$ .

For inhomogeneous deterministic media ( $\nabla c \neq 0$ ;  $c = c(\mathbf{r}, t) = c_0 + \tilde{\alpha}(\mathbf{r}, t)$ , with  $\tilde{\alpha}$  *nonrandom*, for example), operational solutions may be derived directly: all representations of the medium (and boundaries) are equivalent. The resulting solutions provide a possible alternative approach to the current "standard" methods involving partial or parabolic equations (PE) developments [7], [8], at the same time including general arrays, geometries, and signals.

On the other hand, most of the scattering mechanisms in the ocean are essentially random. Accordingly, in these cases, scattering "solutions" are based on the appropriate Langevin equation governing propagation, namely, on the ensemble of representations  $\{\alpha(\mathbf{R}, t)\}$  for which various appropriate probability measures (often nongaussian) are developed, based on both the physics,

\* Based in part on earlier work supported by the Office of Naval Research (1970-1982) and on more recent studies for Codes 10 and 31, NUSC, 1988, 1989. See also [25] herein.

\*\* Contractor, Physics and Applied Mathematics, 127 E. 91 Street, New York, NY 10128, USA.

geometry, and the random mechanisms involved. Thus, practical solutions here are the various moments  $\langle \alpha \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$ , etc., and pdf's  $w_1(\alpha)$ ,  $w_1(\alpha_1, \alpha_2)$ , etc., which are needed, for example, in the calculation of scattering cross sections and subsequent signal processing for target detection and remote sensing [2]–[4].

The desired framework is obtained by recognizing that both the deterministic and random scattered fields in these linear media are representable as four-dimensional feedback systems, with the inhomogeneous portions (including the ocean interfaces) constituting the feedback operations. New features of this work include a combination of diagram methods, perturbational operational series, and equivalent (i.e., deterministic) media operators, which then provide the needed structure for both the direct and moment solutions  $\alpha$ , or  $\langle \alpha_1 \rangle$ , etc., independently, with the latter based on the resultant Dyson and Bethe-Salpeter forms, for  $\langle \alpha \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$ , etc. [2], [3]. Various analytical, iterative, and approximative examples and procedures are briefly presented, to illustrate the desired formal solutions and to provide elements of a framework for computational implementation.

The interfacing between these formally analytic solutions, their software realizations, and the acquisition of (nearly) on-line numerical results remain a major challenge.

## 1. Introduction

Scattering from ocean wave surfaces, volumes, and bottoms is an enduring, central problem not only in underwater acoustics but also in the use of acoustical methods in remote sensing and modeling of the medium itself. Fortunately, in a number of important applications (where first-order Born approximations are adequate), analytic solutions are available (see, for example, recent work of the author [1], [4]).

In many cases, however, strictly analytic methods fail, primarily because of multiple scatter phenomena, which though linear, destroy the reciprocal character of conventional solutions (for ideal media). Moreover, the requirement of effective modeling imposes further complexities: the field nature of the solutions must include the rôle of the transmitting and receiving arrays whereby the system sensors and signal processing itself are suitably coupled to the medium in question, cf. Fig. 1.1 ff. In addition, doppler and gradient effects may also be important. For short ranges velocity gradients in the medium can often be neglected (i.e.,  $\nabla c \cong 0$ ), but for longer ranges they must be carefully taken into account ( $\nabla c \neq 0$ ). Furthermore, geometry plays a critical rôle: platform motion, beam size, structure, and direction, as well as location in the medium, all dictate potential interactions with the wave-surface and bottom boundaries, as Fig. 2.2 indicates, along with the inherently random inhomogeneous effects of the volume itself [3], [4].

We distinguish two main areas of interest: A. *deterministic inhomogeneous media*, where

random variations are largely ignorable vis-à-vis the large-scale deterministic variations, and B. *random inhomogeneous media*, for which significant media variations are stochastic, with and without deterministic components. The former class (A) appears to be so far the one which has received the greatest attention with respect to numerical methods [7], [8], and [9], [10], with attention largely centered on the purely spatially dependent velocity gradient  $\nabla c(r,z) = c_0 + \alpha(r,z)$ . Here, however, in advance of current efforts, we shall direct our attention to the more complex situation (B), where in addition to deterministic variations of  $\nabla c$ , there are important random ones as well. In fact, our treatment will proceed in a general canonical way, allowing for both the deterministic and random variations in the medium, including its important boundaries.

### 1.1 Aims of the Paper

Before numerical procedures can be applied, however, it is necessary to develop the appropriate analytical forms of solution from which in most cases numerical results must be extracted. The aims of this paper, therefore, are to outline an analytical-operational framework for initiating computational solutions to underwater acoustic scattering problems, in particular, which include the relevant ocean surface and bottom boundaries, as well as volume effects.

We emphasize that this paper does not intend to provide explicit computational procedures and solutions: it is rather aimed at providing the "macro-algorithms" from and to which appropriate software may be designed and applied. Our aims include providing formal operational structures, with some special cases in which analytic solutions are obtainable, and which consequently require a lower order of computational effort and sophistication. A collateral aim of this work is to entice interest in pursuing a computational formulation, based on the various formal operational "solutions" derived here for the composite deterministic and random fields  $\alpha(R,t)$ , namely  $\langle \alpha \rangle$ , cf. (2.33), and higher-order moments  $\langle \alpha_1 \alpha_2 \rangle$ , etc. Our approach here is a "top-down" approach, in which we start with as general a formulation as possible, consistent with the broad class of problems embodied in the propagation and processing schema of Fig. 1.1 and the geometries of Fig. 2.1 ff. We proceed then to more specialized cases. This reveals the embedding of the latter in the generality of the former, and thus provides a "perspective" for specific medium models.

### 1.2 New Elements

Among the new features of the present paper are

- (1) Formal operational formulations which can provide the basis for a large-scale computational attack on these four-dimensional scattering problems, Sec. 2.
- (2) A feedback operational method for obtaining the (first-order) equivalent medium renormalization operator, cf. (2.34), by means of a converging series of estimates, Sec. 3.3.

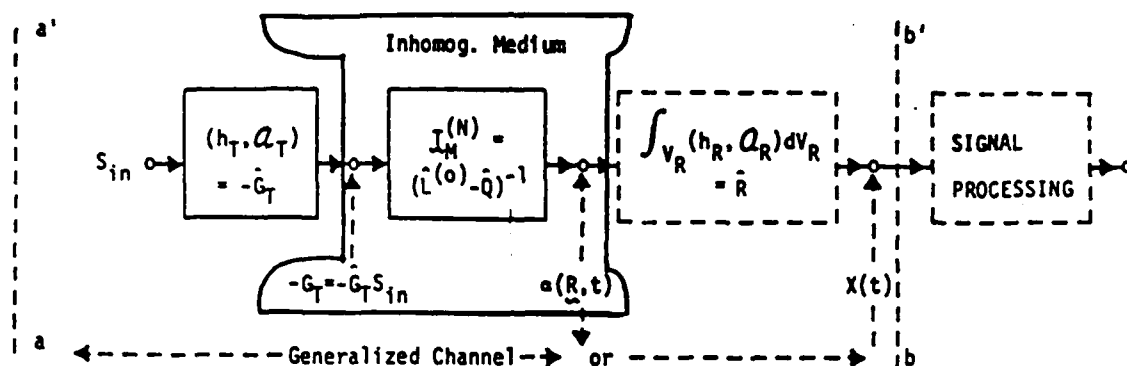


Fig. 1.1 Operational schematic of an inhomogeneous (linear) medium, with source and receiver coupling. Here  $\hat{Q}$  is the inhomogeneity operator associated with this general inhomogeneous (linear) medium.

- (3) Some fully analytic solutions in important special cases, e.g., infinite or "weakly-bounded" media, where in effect there is negligible interaction between sources, boundaries, and among the different scattering modes (Surface, Volume, Bottom), Sec. 2.7.
- (4) Various explicit physical scattering models for the inhomogeneity operator  $\hat{Q}$ , including the important wind-wave scattering cases, Eqs. (2.31).
- (5) A hierarchy of approximations for the equivalent deterministic inhomogeneity operator  $\hat{Q}^{(d)}$ , which apply in different physical situations, Sec. 2.5.

### 1.3 Organization

Accordingly, the present paper is organized in the following general but concise fashion: Section 2 introduces formal operational solutions, which form the basis for the treatment of both deterministic and random media. In Section 3 various diagram methods and solution equivalents are presented, first for the deterministic cases and then for the many situations involving random media components. Useful approximations are next briefly described in this section, along with a possible method for estimating the renormalization operators. Section 4 completes the paper with a



discussion of the interfacing problems between the analytic/operational and computational formulations by reviewing via the text the main steps leading up to the as yet unachieved software realizations.

## 2. Formal Operational Solutions

Accordingly, the above discussion indicates the critical need, at some point, for numerical procedures to obtain the needed quantitative description of the received acoustic field, for whatever operational or oceanographic purpose at hand.

What are the needed descriptors of this received field? This will, of course, depend on whether or not there are significant random, as well as deterministic inhomogeneities in the medium. Here we shall assume a (linear) combination of both types, which permits us to focus on one or the other as limiting cases. Thus, in general we can write formally for the inhomogeneity operator  $\hat{Q}$ , cf. Fig. 1.1

$$\hat{Q} = \hat{Q}^{(h)} + \hat{Q}^{(l)}, \quad (2.1)$$

where  $\hat{Q}^{(h)}$ ,  $\hat{Q}^{(l)}$  are respectively associated with the deterministic and random parts. For example,  $\hat{Q}^{(h)}$  usually dominates in a nonzero-gradient ocean with small surface interactions (cf. some of the current treatments [7]–[10]), while  $\hat{Q}^{(l)}$  is most significant in surface or bottom scatter situations, at comparatively short ranges and high frequencies, where  $\nabla c \neq 0$  often, cf. [1], [4].

Now, since the medium, including its boundaries, is both spatially and temporally stochastic in general, "solutions" to the appropriate propagation equations for the input, incident, and scattered fields are necessarily *statistics* of these fields, namely, means, variances, covariances, higher-order moments, and finally, various orders of the *probability distributions* of these fields. Thus, if  $\alpha(\mathbf{R}, t)$  represents the (acoustic) field at point  $(\mathbf{R}, t)$  in this random, inhomogeneous medium, one seeks  $\langle \alpha \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$  ( $= \langle \alpha(\mathbf{R}_1, t_1) \alpha(\mathbf{R}_2, t_2) \rangle$ ),  $\langle \alpha_1 \alpha_2 \alpha_3 \rangle$ , etc., and more completely,  $w_1(\alpha_1)$ ,  $w_2(\alpha_1, \alpha_2)$ , etc. The lower order moments, for example,  $\langle \alpha_1 \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$ , are needed in obtaining the scattering cross-sections of the "illuminated" wave-surface or bottom, cf. Fig. 2.1, while  $w_1(\alpha_1)$  is required for signal processing (cf. Part II of [4]). What makes the latter critically non-trivial is the fact that  $\alpha$  is often strongly *nongaussian* (cf. VI of [4]). Even in the cases where the Central Limit Theorem applies (cf. Sec. 7.7 of [5], for example), so that the field is gaussian, one still needs the lower-order moments  $\langle \alpha \rangle$ ,  $\langle \alpha_1 \alpha_2 \rangle$ , in order to specify the gaussian process,  $\alpha(\mathbf{R}, t)$ .

### 2.1 Formal Development

Clearly, for realistic solutions, many complicating effects must be included, which almost always at some point makes a computational effort essential. Initially, one starts with a

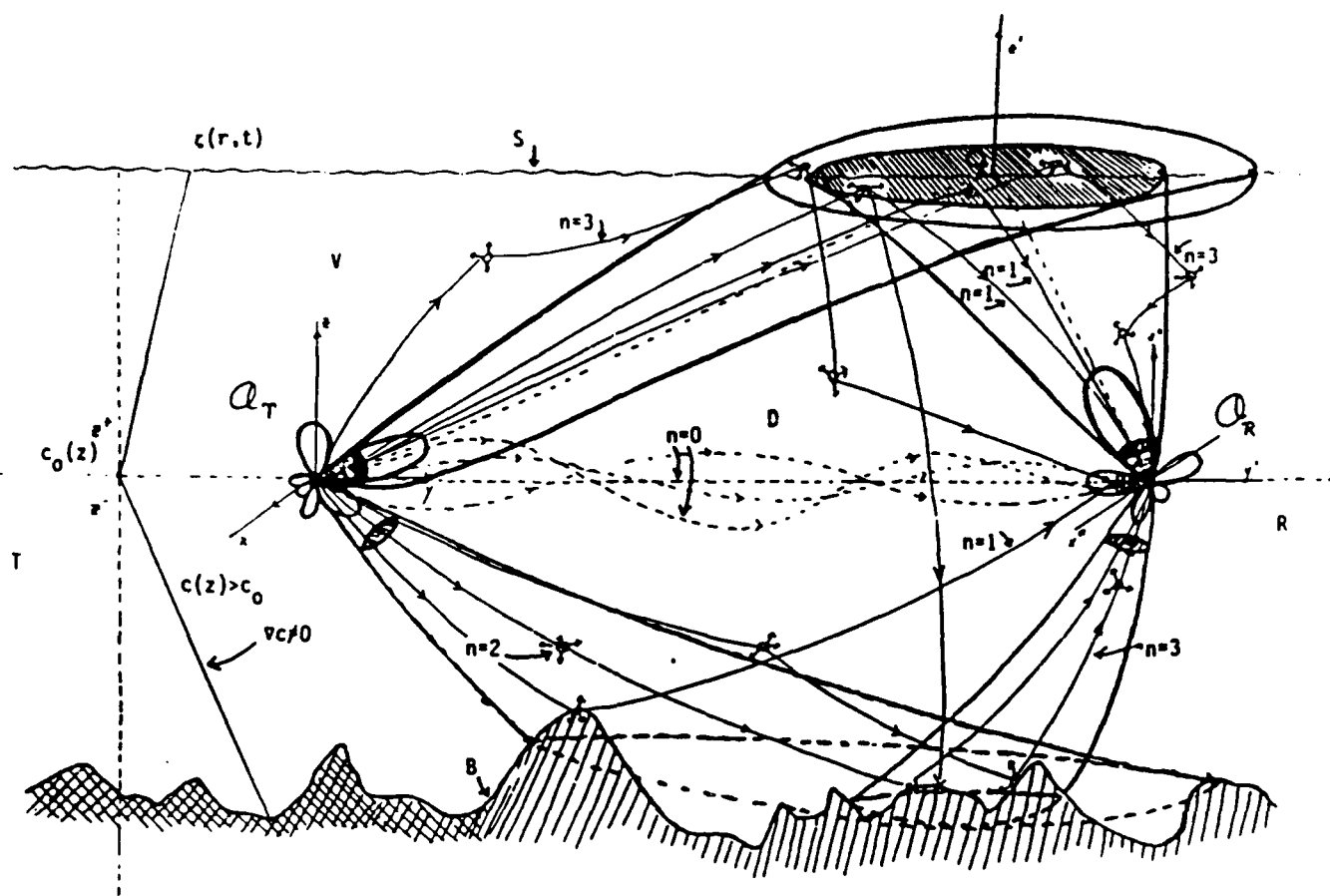


Fig. 2.1 Schematic scatter channel geometry of source ( $T$ ), medium ( $V$ ), and boundaries ( $S, B$ ), with receiver ( $R$ ),  $D$  = unscattered, or "direct" path, and  $n$  is the order of the interactions. Sufficiently high frequencies are assumed to permit illustrative ray paths.

propagation equation which at least implicitly contains the major physical phenomena governing the generation and development of both the scattered and unscattered fields. Formally, for the linear media assumed here, the propagated field  $\alpha(R, t)$  obeys a partial integro-differential equation of the form

$$(\hat{L}^{(0)} - \hat{Q})\alpha = -G_T + [\text{b.c.'s} + \text{i.c.'s}].$$

(2.2)

Here  $G_T$  is the source function, e.g.,  $G_T = \hat{G}_T S_{in}$ , cf. Fig. 1.1, and  $\hat{L}^{(0)}$  is a linear (scalar) partial differential operator, where  $\hat{L}^{(0)}$  is associated with the homogeneous portion of the medium. In

(2.2),  $\hat{Q}$  is, generally, a (scalar, linear) integro-differential scattering operator, which describes the interaction of the incident, i.e., homogeneous field with the differential, or local, scattering elements of the inhomogeneous portion of the medium. (The possible integral operator component of  $\hat{Q}$  stems from local scatterer doppler effects, for example.) Here, *b.c.'s* = boundary conditions, and *i.c.'s* = initial conditions. Since, formally from (2.2)  $\alpha = (\hat{L}^{(0)} - \hat{Q})^{-1}(-G_T)|_{b.c.+i.c.}$ , from  $\alpha = T_M^{(N)}(-G_T)$ , cf. Fig. 1.1, one has directly

$$T_M^{(N)} = (\hat{L}^{(0)} - \hat{Q})^{-1} \quad (2.3)$$

for the medium operator  $T_M^{(N)}$ , now expressed in terms of the homogeneous and inhomogeneous components of the medium.

Because of the usual statistical nature of  $\hat{Q}$ , Eq. (2.2) is really an ensemble of equations, which is called the (associated) *Langevin Equation* [cf. Chapter 10 of [5]], which can be written as

$$\{(\hat{L}^{(0)} - \hat{Q})\alpha = -G_T + (b.c.'s + i.c.'s)\}, \quad (2.4)$$

where the brackets { } emphasize the ensemble character of this Langevin equation. In subsequent discussion the brackets may be omitted for convenience, it being noted that  $\hat{Q}$ , and therefore  $\alpha$ , are stochastic. (See Sec. IIB of [4] for remarks.)

An important example for acoustic propagation in underwater media is the case of inhomogeneous absorptive media [3], for which (2.2) is specifically [11]

$$\left\{ \left( 1 + \tau_x(r,t) \frac{\partial}{\partial t} \right) \nabla^2 - \frac{1}{c_0^2} [(1 + \epsilon(R,t)) \frac{\partial^2}{\partial t^2}] \right\} \alpha = -G_T \quad (2.5a)$$

where

$$\begin{aligned} \therefore \hat{L}^{(0)} &\equiv \left( 1 + \tau_{ox} \frac{\partial}{\partial t} \right) \nabla^2 - \frac{1}{c_0^2} \frac{\partial^2}{\partial t^2} \\ \hat{Q} &\equiv \frac{\epsilon}{c_0^2} \frac{\partial^2}{\partial t^2} - \tau_{ox} \gamma_x \frac{\partial}{\partial t} \nabla^2 \end{aligned} \quad (2.5b)$$

with  $\tau_x \equiv \tau_{ox} (1 + \gamma_x(r,t))$  generally. When  $\tau_{ox} = 0$ , (2.5a) reduces to the more familiar "extended" Helmholtz equation

$$\left\{ \nabla^2 - \frac{1}{c_0^2} [(1 + \epsilon(R,t)) \frac{\partial^2}{\partial t^2}] \right\} \alpha = -G_T \quad (2.6)$$

with

$$\hat{Q} = \frac{\epsilon}{c_0^2} \frac{\partial^2}{\partial t^2}; \quad \hat{L}^{(0)} \equiv \nabla^2 - \frac{1}{c_0^2} \frac{\partial^2}{\partial t^2}, \quad (2.6a)$$

where

$$\mathbf{R} = \hat{i}_x x + \hat{i}_y y + \hat{i}_z z, \quad (2.7)$$

and rectangular coördinates are assumed throughout, so that  $\nabla \cdot \nabla = \nabla^2$ , etc. Specifically,  $c_0 =$  (constant) wavefront speed,  $\epsilon$  embodies the effects of velocity gradients, internal wave phenomena, and/or (weak) local turbulence, while  $\tau_x$  represents the effects of relaxation absorption (due to  $\text{Mg}_2\text{SO}_4$  and other salts).

Similarly, in the more restricted situations where (2.6) is replaced by a purely deterministic model in which  $\epsilon(\mathbf{R}, t) \rightarrow \epsilon(\mathbf{R})$  is nonrandom, this Helmholtz equation can be approximated (at a given frequency  $f_0$ ) by a basic form of the *parabolic equation* (PE), which is expressed by (Eq. (2.34), [8]), in cylindrical coördinates [ $\mathbf{R} = (r, z) = (r, \theta, z)$ ]:

$$\frac{\partial \alpha_0}{\partial r} = \left( A + B \frac{\partial^2}{\partial z^2} \right) \alpha_0; \quad \alpha_0 = \alpha_0(\mathbf{R}), \quad (2.8)$$

where specifically

$$A \equiv \frac{i}{2} k_0 [n^2(r, z) - 1]; \quad B \equiv \frac{i}{2k_0}; \quad k_0 = \omega_0/c_0 = 2\pi f_0/c_0, \quad (2.8a)$$

$$n^2 = (1 + \epsilon). \quad (2.8b)$$

Comparing (2.2) and (2.8) gives at once here

$$\hat{L}^{(0)} = B \frac{\partial^2}{\partial z^2} - \frac{\partial}{\partial r}; \quad \hat{Q} = A_\epsilon \hat{I} = [-ik_0 \epsilon / 2] \hat{I} \quad (2.9)$$

where  $\hat{I}$  = unit operator,  $\hat{I}C = C$ , etc., and  $\hat{L}^{(0)} \alpha_0 = 0$  is an equation of the Schrödinger type since  $B$  is purely imaginary.

The formal solution of the Langevin equation (2.4) is obtained from the equivalent operational form

$$(\hat{I} - \hat{M}\hat{Q})\alpha = \hat{M}(-G_T); \quad \alpha = \alpha_H + \alpha_I; \quad \alpha_H \equiv \hat{M}(-G_T), \quad (2.10)$$

where  $\alpha_H$  is the homogeneous (i.e., non-scattered) component of the total field  $\alpha$ , with  $\alpha_i$  the associated inhomogeneous (scattered) field.  $\hat{M}$  is  $\hat{L}^{(0)-1}$ , with the boundary and initial conditions; in fact,  $\hat{M}$  is the integral Green's function operator

$$\hat{M}(\mathbf{R}, t | \mathbf{R}', t') \equiv - \int_{-\infty}^{\infty} dt' \int d\mathbf{R}' g(\mathbf{R}, t | \mathbf{R}', t') (\cdot)_{\mathbf{R}', t'} \quad (2.11)$$

obtained from  $\hat{L}^{(0)}g = -\delta(\mathbf{R}-\mathbf{R}')\delta(t-t')$ . The formal operational solution of (2.10) now becomes

$$\alpha = (\hat{1} - \hat{\eta})^{-1} \alpha_H, \quad \hat{\eta} \equiv \hat{M}\hat{Q}.$$

(2.12)

Here  $\hat{\eta}$  is the *field renormalization operator* (FRO), and (2.12) represents the *Feedback Operational Solution* (FOS) for  $\alpha$ , c.f. remarks following Eq. (2.35) et seq. Expansion of (2.12) yields the *Perturbation Theoretical Series Solution* (PTSS)

$$\alpha = \alpha_H + \sum_{n=1} \hat{\eta}^{(n)} \alpha_H; \quad \|\hat{\eta}\| < 1,$$

(2.13)

where  $\hat{\eta}^{(n)} = [\hat{\eta}\hat{\eta}\dots\hat{\eta}]_n$  is the  $n^{\text{th}}$ -iteration of  $\hat{\eta}$  and where the operator formalism used here is represented explicitly by

$$(\hat{A})^{(n)} = \hat{A}^{(n)} \equiv \hat{A}(\mathbf{R}, t | \mathbf{R}', t') \hat{A}(\mathbf{R}', t' | \mathbf{R}'', t'') \dots \hat{A}(\mathbf{R}^{(n-1)}, t^{(n-1)} | \mathbf{R}^{(n)}, t^{(n)}) \quad (2.13a)$$

which is generally distinct from the *direct operator product*

$$\hat{A}^n \equiv \hat{A}(\mathbf{R}, t | \mathbf{R}', t') \hat{A}(\mathbf{R}, t | \mathbf{R}'', t'') \dots \hat{A}(\mathbf{R}, t | \mathbf{R}^{(n)}, t^{(n)}) \quad (2.13b)$$

and its more general form

$$\hat{A}_1 \dots \hat{A}^n = \hat{A}(\mathbf{R}, t | \mathbf{R}', t') \dots \hat{A}(\mathbf{R}_n, t_n | \mathbf{R}^{(n)}, t^{(n)}). \quad (2.13c)$$

We have also the conventions

$$\left. \begin{aligned} \hat{A}_1 \hat{B}_1 &= \hat{A}(\mathbf{R}_1, t_1 | \mathbf{R}', t') \hat{B}(\mathbf{R}_1, t_1 | \mathbf{R}'', t'') \\ \hat{A}_1 \hat{B}_2 &= \hat{A}(\mathbf{R}_1, t_1 | \mathbf{R}', t') \hat{B}(\mathbf{R}_2, t_2 | \mathbf{R}'', t'') \end{aligned} \right\} \quad (2.13d)$$

so that clearly  $\hat{A}_1 \hat{B}_2 \neq \hat{B}_2 \hat{A}_1$ , i.e.,  $\hat{A}_1, \hat{B}_2$  do not commute, unless the operand is symmetric.

## 2.2 Some Homogeneous Methods and Results

For the usual cases where there is negligible interaction of the medium and boundaries upon the *source*, we can replace  $\hat{M}$  by  $\hat{M}_\infty$ , where  $\hat{M}_\infty$  is the integral Green's function operator for the associated infinite homogeneous medium. Then, also, we have  $\hat{\eta} \rightarrow \hat{\eta}_\infty = \hat{M}_\infty \hat{Q}$ , cf. (2.12).

Next, to proceed further it is clear from (2.12) that we must determine the homogeneous field  $\alpha_H$ ,  $\hat{\eta}_\infty = 0$ , or  $\hat{Q} = 0$ , now. In the light of the fact that media boundaries or interfaces can be equivalently considered as (distributed) inhomogeneities in an otherwise homogeneous medium, cf. Sec. 2.4 ff., to obtain solutions in the homogeneous cases we must therefore consider *unbounded* media, along with the condition  $\hat{Q} = 0$ . More precisely, by "unbounded" we mean the infinite spatial domain exclusive of sources.

The general method of solution here (including bounded media) involves two steps:

- I. Obtain the associated Green's function,  $g$ , from (2.2), ( $\hat{Q} = 0$ );
- II. Construct the corresponding GHP (Generalized Huygen's Principle) [20],

} (2.14)

and thereby obtain the field,  $\alpha$ . For unbounded homogeneous media this is easily done. Thus, the Green's function  $g_\infty$  is found from the defining relation

$$\hat{L}^{(0)} g_\infty = -\delta(t-t') \delta(\mathbf{R}-\mathbf{R}'), \quad (2.14a)$$

or

$$g(\mathbf{R}, t | \mathbf{R}', t')_\infty = -\hat{M}_\infty \delta_{t'} \delta_{\mathbf{R}' \mathbf{R}'}, \quad (2.14b)$$

where  $\hat{M}_\infty$  is the inverse (integral) operator to  $\hat{L}^{(0)}$  + i.c.'s, with  $\hat{M}_\infty^{-1} = \hat{L}^{(0)}$ . Integrating over  $(\mathbf{R}', t')$  shows at once that  $\hat{M}_\infty$  and  $g_\infty$  are related here by

$$\begin{aligned} \hat{M}(\mathbf{R}, t | \mathbf{R}', t')_\infty &= - \int_{-\infty}^{\infty} dt' \int_{(\infty)} d\mathbf{R}' g(\mathbf{R}, t | \mathbf{R}', t')_\infty (\cdot)_{\mathbf{R}', t'} \\ &= 0, \quad t \leq t' - , \end{aligned} \quad (2.15)$$

where, by causality,  $g_{\infty} = 0$ ,  $t \leq t' -$ , which represents the initial condition (i.c.) on the "point"-source in (2.14a). Thus,  $\hat{M}_{\infty}$  is now the *Green's function operator*, with the kernel  $g_{\infty}$ .

The desired field  $\alpha(\mathbf{R}, t)_{\infty}$  is found directly from (2.2) ( $\hat{Q}$ , b.c.'s = 0), viz.:

$$\hat{L}^{(0)}\alpha_{\infty} = -G_T, \text{ or} \quad (2.16a)$$

$$\alpha(\mathbf{R}, t)_{\infty} = \hat{M}_{\infty}(-G_T) = \int_{-\infty}^{\infty} dt' \int_{V_T} G_T(\mathbf{R}', t') g(\mathbf{R}, t | \mathbf{R}', t')_{\infty} d\mathbf{R}' \quad (2.16b)$$

$$= \int_{-\infty}^{\infty} dt' \hat{G}_T(g_{\infty} S_{in}) = \int_{-\infty}^{\infty} T_{AT} S_{in} dt', \quad (2.16c)$$

where  $G_T = 0$ ,  $t' \leq t_0 -$ ,  $\mathbf{R} \neq V_T$ : the source function is initiated at  $t' = t_0$  and occupies the domain  $V_T(<\infty)$ . The relations (2.16b,c) are the simplest form of GHP here for homogeneous unbounded media (outside the source domain).

Various transform equivalents of  $\hat{M}_{\infty}$  prove useful. These may be expressed as follows, from (2.16b):

$$\hat{M}_{\infty} = -\mathcal{F}_s^{-1} \left\{ \int_{-\infty}^{\infty} dt' \int_{(\infty)} Y_0(\mathbf{R}, s | \mathbf{R}', t')_{\infty} (\cdot)_{\mathbf{R}', t'} d\mathbf{R}' \right\} \equiv -\mathcal{F}_s^{-1} \{Y_{0,\infty}\} \quad (2.17a)$$

$$= -\mathcal{F}_k \mathcal{F}_s^{-1} \left\{ \int_{-\infty}^{\infty} dt' \int_{(\infty)} Y_0(\mathbf{k}, s | \mathbf{R}', t')_{\infty} (\cdot)_{\mathbf{R}', t'} d\mathbf{R}' \right\} \equiv -\mathcal{F}_k \mathcal{F}_s^{-1} \{\hat{\mathcal{Y}}_{0,\infty}\} \quad (2.17b)$$

$$= -\mathcal{F}_k \mathcal{F}_s^{-1} \left\{ \mathcal{Y}_0(\mathbf{k}, s)_{\infty} \int_{-\infty}^{\infty} dt' \int_{(\infty)} e^{-i\mathbf{k} \cdot \mathbf{R}' - st'} (\cdot)_{\mathbf{R}', t'} d\mathbf{R}' \right\} \quad (2.17c)$$

where (2.17a-c) define the transformed operators  $\hat{Y}_{0,\infty}$ ,  $\hat{\mathcal{Y}}_{0,\infty} (= \hat{\mathcal{Y}}_0(\mathbf{k}, s | \mathbf{R}', t')_{\infty})$  respectively, and where  $\mathcal{F}_t \{\hat{M}_{\infty}\} = -\hat{Y}_{0,\infty}$ ,  $\mathcal{F}_R^{-1} \mathcal{F}_t \{\hat{M}_{\infty}\} = -\hat{\mathcal{Y}}_0(\mathbf{k}, s | \mathbf{R}', t')$  are the corresponding inverses.

The general transform relations are explicitly

$$a(t-t') = \mathcal{F}_s^{-1} \{e^{-st'} A(s)\} = \begin{matrix} \infty + d(>0) \\ \text{Br}_1 = -\infty + d \end{matrix} \int A(s) e^{s(t-t')} \frac{ds}{2\pi i} \neq 0, \quad t > t' - \\ = 0, \quad t \leq t' - \quad (2.18a)$$

where  $s$  is a complex (angular) frequency, and provided all the singularities of  $A(s)$  lie in  $\text{Re}(s) < d$ ;  $a = 0$ ,  $t \leq t' -$  is, of course, an initial condition (i.c.). The inverse of (2.18a) is

$$e^{-st'} A(s) = \mathcal{F}_t \{a(t-t')\} = \int_{-\infty}^{\infty} e^{-st} a(t-t') dt = e^{-st'} \int_{-\infty}^{\infty} e^{-s\tau} a(\tau) d\tau, \quad \text{Re}(s) > 0. \quad (2.18b)$$

In the steady-state régime ( $t' \rightarrow -\infty$ ) we choose  $d = 0$  and use  $s = i\omega = 2\pi if$ , where  $(\omega, f)$  are real frequencies, with an appropriate indentation of the contour ( $Br_1, d=0$ ) for any singularities on  $\text{Re}(s) = 0$ . The contour  $BR_1$  is a Bromwich contour [26]. Similarly,  $\mathcal{F}_R^{-1}$ ,  $\mathcal{F}_k$  are spatial Fourier transforms, e.g.,

$$\begin{aligned} B(\mathbf{k}) &= \mathcal{F}_R^{-1} \{b(\mathbf{R})\} = \int_{[\mathbf{R}]} e^{-i\mathbf{k} \cdot \mathbf{R}} b(\mathbf{R}) d\mathbf{R}; \\ b(\mathbf{R}) &= \mathcal{F}_k \{B(\mathbf{k})\} = \int_{(\mathbf{k})} e^{i\mathbf{k} \cdot \mathbf{R}} B(\mathbf{k}) \frac{d\mathbf{k}}{(2\pi)^3} \end{aligned} \quad (2.18c)$$

where, as before, cf. (2.7),  $\mathbf{k} = \hat{\mathbf{i}}_x k_x + \hat{\mathbf{i}}_y k_y + \hat{\mathbf{i}}_z k_z (= 2\pi v)$  is a *vector wave number* (and  $v$  is a *vector spatial frequency*). Multiple transforms of quantities like  $C(\mathbf{R}, t)$  are handled in the same way, cf. (2.17b,c).

For those unbounded media—unbounded in the sense that a propagating wave front never encounters a bounding surface—the evaluation of the Green's function  $g_\infty$  from (2.14a) and the general field from (2.16) is readily accomplished. From (2.14a) one has

$$\mathcal{F}_R^{-1} \mathcal{F}_t \hat{L}^{(0)} \{ \mathcal{F}_s^{-1} \mathcal{F}_k \{g_{0,\infty}\} \} = -e^{-i\mathbf{k} \cdot \mathbf{R}' - st'}, \quad (2.19a)$$

$$\therefore g_{0,\infty} = g_0(\mathbf{k}, s | \mathbf{R}', t')_\infty = -L_0(\mathbf{k}, s)^{-1} e^{-i\mathbf{k} \cdot \mathbf{R}' - st'}, \quad (2.19b)$$

where  $L_0(\mathbf{k}, s)$  is the result of applying  $\hat{L}^{(0)}$  to  $\mathcal{F}_s^{-1} \mathcal{F}_k$ , remembering that  $\nabla e^{i\mathbf{k} \cdot \mathbf{R}} = i\mathbf{k} e^{i\mathbf{k} \cdot \mathbf{R}}$ ,  $\nabla^2 e^{i\mathbf{k} \cdot \mathbf{R}} = -\mathbf{k} \cdot \mathbf{k} e^{i\mathbf{k} \cdot \mathbf{R}} = -k^2 e^{i\mathbf{k} \cdot \mathbf{R}}$ ,  $\frac{\partial}{\partial t} e^{st} = s e^{st}$ , etc. In fact, one has

$$\boxed{-L_0(\mathbf{k}, s)^{-1} = \mathcal{G}_0(\mathbf{k}, s)_\infty} \quad (2.20)$$

cf. (2.17b,c) so that, from (2.19b),

$$g(\mathbf{R}, t | \mathbf{R}', t')_\infty = \mathcal{F}_s^{-1} \mathcal{F}_k \{g_{0,\infty}\} = \int_{Br_1} e^{s(t-t')} \frac{ds}{2\pi i} \int_{[\mathbf{k}]} e^{i\mathbf{k} \cdot (\mathbf{R}-\mathbf{R}')} \{-L_0(\mathbf{k}, s)^{-1}\} \frac{d\mathbf{k}}{(2\pi)^3}. \quad (2.21a)$$

This can be put in the more convenient equivalent form for evaluation with the help of spherical coordinates:  $\mathbf{k} = (k, w [= \cos \theta], \phi)$ , viz.:



$$g(\mathbf{R}, t | \mathbf{R}', t')_{\infty} = \int_{B_{r_1}} e^{s(t-t')} \frac{ds}{2\pi i} \frac{1}{(2\pi)^3} \int_0^{\infty} k^2 dk \int_{-1}^1 dw \cdot \int_0^{2\pi} [-L_0(\mathbf{k}, s)]^{-1} e^{i\mathbf{k}|\mathbf{R}-\mathbf{R}'|w} d\phi. \quad (2.21b)$$

#### A. Conditions:

Various conditions and properties of (2.21b) are now noted:

(i). "*Spatial causality*": this is the *radiation condition* [15]

$$\lim_{R \rightarrow \infty} \left( \left\{ \begin{array}{c} R \frac{\partial}{\partial R} \\ R_{ik} \end{array} \right\} + \frac{R}{R} \left\{ \begin{array}{c} \frac{1}{c_0} \frac{\partial}{\partial t} \\ \frac{s}{c_0} \end{array} \right\} \right) \left\{ \begin{array}{c} g_{\infty} \\ Y_{0,\infty} \end{array} \right\} = 0, \quad R = |\mathbf{R}|, \quad (2.22)$$

which ensures that only outgoing waves from the source ( $\epsilon V_T$ ) are propagated. This spatial causality condition is used in the specific evaluation of  $g_{0,\infty}$ , (2.21b), by appropriate modifications  $C_k$  of the  $k$ -contour  $(-\infty, \infty)$  to include only singularities in the complex  $k$ -plane which yield the required outgoing waves.

(ii). "*Temporal causality*": this is the well-known condition that propagation cannot occur before the source initiating it is activated, cf. (2.15), (2.18), or more precisely, that events cannot occur (macroscopically) at some point  $P(\mathbf{R}, t)$  before the source has been initiated and the field generated in the medium has reached the point in question. For causality in time one has the *Paley-Wiener criterion* [5], pp. 96, 97, 102 and Refs. Here ( $s \rightarrow i\omega$ ):

$$J \equiv \int_0^{\infty} \frac{\log |Y_0(\mathbf{R}, i\omega | \mathbf{R}')_{\infty}|^2}{1 + \omega^2} d\omega < \infty, \quad (2.23)$$

where specifically

$$Y_0(\mathbf{R}, s | \mathbf{R}')_{\infty} = \mathcal{F}_t \{ g(\mathbf{R}, s | \mathbf{R}', t')_{\infty} e^{st'} \} = Y_0(\mathbf{R}, s | \mathbf{R}', t')_{\infty} e^{st'}, \quad (2.23a)$$

$$= \frac{1}{(2\pi)^3} \int_0^{\infty} k^2 dk \int_{-1}^1 dw \int_0^{2\pi} [-L_0(\mathbf{k}, s)]^{-1} e^{i\mathbf{k}|\mathbf{R}-\mathbf{R}'|w} d\phi, \quad (2.23b)$$

from (2.21b), (2.17a). This condition is obeyed generally, from the initial condition on  $g$ , cf.

(2.15). The combination of (2.22) and (2.23) is the full, space-time causality condition, which when axiomatically invoked (as it is here) ensures that only time-related solutions of (2.16) are possible.

(iii). *Reciprocity*: the point source [in (2.14a)] and the observer [at  $P(R,t)$ ] are interchangeable in the Green's function, provided temporal causality [(ii) above] is also obeyed. Thus, one has  $R' \rightarrow R$ ,  $R \rightarrow R'$  and  $t \rightarrow -t'$ ,  $t' \rightarrow -t$ , so that  $g(R', -t' | R, -t)$ . From (2.21) it is at once evident that reciprocity for these homogeneous media is obeyed.

(iv). *"Regularity at infinity"*: [15] this ensures that  $|g_\infty| (\leq \infty)$ , i.e., is bounded as  $R \rightarrow \infty$ ; (this is *not* necessarily guaranteed by (2.22)). This condition is a reflection of the fact that the (point-) source has bounded energy and consequently its field ( $g_\infty$ ) must have also, all  $R$ .

Not too surprisingly from the above, we may now regard these homogeneous linear media as being, in effect, *linear space-time filters*. In the language of modern circuit theory the Green's function,  $g_\infty$ , represents the medium's *weighting function*;  $Y_{0,\infty}$ ,  $\mathcal{Y}_{0,\infty}$  correspond to the frequency-, and frequency-wave number *system functions*, or "filter" *spectral densities*, of this causal, space-time filter, where the governing space-time causality condition is the combination of (i) and (ii) above, cf. (2.22), (2.23). However, unlike conventional, "lumped-element" circuit models, these "circuits" (i.e., the medium) are in effect composed of a continuum of elements, distributed throughout space. The dynamical ("circuit") equations of the latter are *partial* differential equations, obeying boundary conditions (here as  $R \rightarrow \infty$ , cf. (2.22)) as well as initial conditions, while the former are limited to ordinary differential equations, subject only to initial conditions; (both obey appropriate stability conditions, (iv), for example), [27]. Further critical differences appear when the medium becomes inhomogeneous, and random [cf. Sec. 2.4 ff.].

For the Helmholtz case (2.6), (2.6a),  $\hat{Q} = 0$ , it is easily seen that (2.11) becomes (2.15), and that following the methods described in (2.16)–(2.18) one gets specifically for with the Green's function now

$$g_\infty = \delta(\Delta t - \rho/c_0)/4\pi\rho ; \quad \rho = |R - R'|, \quad \Delta t = t - t'. \quad (2.24)$$

Similarly, it is also found [3] that when  $\hat{Q} = 0$ ,  $\hat{M} \rightarrow \hat{M}_\infty$ , the solution of (2.5a) reduces to

$$g(R,t | R',t')_\infty = F_k F_s^{-1} \{ \hat{\mathcal{Y}}_{0,\infty} \} = F_s^{-1} \{ \hat{Y}_{0,\infty} \}, \quad (2.25a)$$

where  $F$ , etc. denote Fourier transforms, with

$$\hat{\mathcal{Y}}_{0,\infty} = \mathcal{Y}_0(k,s) \int_{(-\infty)}^{\infty} dt' \int e^{-ik \cdot R' - st'} ( )_{R',t'} dR' = -F_R^{-1} F_t \{ \hat{M}_\infty \}, \quad (2.25b)$$

$$\mathcal{Y}_0(\mathbf{k}, s)_\infty = [k^2(1 + \tau_{ox}s) + s^2/c_o^2]^{-1}. \quad (2.25c)$$

It can be shown that here [6]

$$\hat{Y}_{0,\infty} = \frac{e^{-(\rho s/c_o)(1 + \tau_{ox}s)^{-1/2} - st'}}{4\pi\rho(1 + \tau_{ox}s)} \quad (2.26a)$$

and that now, explicitly,

$$g_\infty = \frac{1}{4\pi\rho\tau_{ox}} \left\{ 1 - \frac{1}{\sqrt{\pi}} \sum_{n=0}^{\infty} \frac{(-1)^n (1/2)_n}{(2n+1)!} \left( \frac{\rho}{c_o \sqrt{\tau_{ox}\Delta t}} \right)^{2n+1} e^{-\Delta t/\tau_{ox}} {}_1F_1(-1-2n; \frac{1}{2} - n; \Delta t/\tau_{ox}) \right\} \quad (2.26b)$$

for the Green's function of the associated unbounded medium, where  ${}_1F_1$  is a confluent hypergeometric function.

Finally, in the case of the PE approximation (2.8) above, one can show that the Green's function associated with (2.9) is

$$g(\mathbf{r}, z | \mathbf{r}', z')_\infty = \frac{-ik_o}{2\pi\Delta r} e^{ik\Delta z^2/2\Delta r}, \quad \Delta r = r - r'. \quad (2.27)$$

With a *gaussian beam* for the source (along  $z$ ) for these narrow angles, e.g.,

$$G_T = A_o e^{-z^2/a^2}, \quad (2.28)$$

the associated homogeneous field  $\alpha_{oH}$  is found to be [19]

$$\alpha_{oH}(\Delta r, z) = \int g(\mathbf{r}, z | \mathbf{r}', z')_\infty G_T(z') dz', \quad (2.29a)$$

$$= \frac{ak_o A_o}{(4\Delta r^2 + k_o^2 a^4)^{1/2}} \exp \left[ -\frac{k_o^2 a^2 z^2}{4\Delta r^2 + k_o^2 a^4} + i \left( \frac{2\Delta r k_o z^2}{4\Delta r^2 + k_o^2 a^4} - \tan^{-1} \frac{2\Delta r}{k_o^2 a^2} \right) \right], \quad (2.29b)$$

which shows the expected  $(\Delta r)^{-1}$  fall-off as  $\Delta r \rightarrow \infty$ .

### 2.3 The FOR

The result (2.12) above can be expressed formally in terms of a generalized *feedback loop*, as shown in Fig. 2.2. Thus, (2.12) can be regarded as an extension of conventional control theory, now to *deterministic* inhomogeneous media for the moment, cf. Sec. 2.4 ff. We call Fig.

2.2 the *feedback operational representation* (FOR) for the FOS, (2.12). Equation (2.13) above is the associated PTSS.

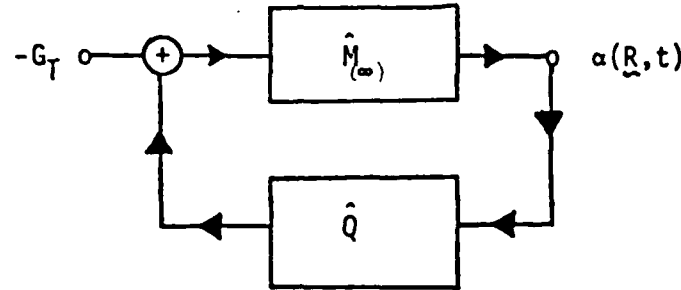


Fig. 2.2 *Feedback Operational Representation (FOR) for the propagated field  $\alpha$ , Eq. (2.12), for linear inhomogeneous media.*

#### 2.4 The Inhomogeneous Operators $\hat{Q}$

These operators embody the various inhomogeneities characteristic of the medium, including its boundaries. Thus, for a typical propagation scenario, sketched in Fig. 2.1, we may express  $\hat{Q}$ , (2.1), in more detail for these linear media as a combination of scattering modes:

$$\hat{Q} = \hat{Q}_S + \hat{Q}_V + \hat{Q}_B = [\hat{Q}_S^{(h)} + \hat{Q}_S^{(I)}] + [\hat{Q}_V^{(h)} + \hat{Q}_V^{(I)}] + [\hat{Q}_B^{(h)} + \hat{Q}_B^{(I)}] \quad (2.30)$$

where S, V, B, respectively, denote the surface, volume, and bottom in this instance, and (h), (I), designate the deterministic and (purely) random components of each associated operator, cf. (2.1).

As examples, we have explicitly from the various acoustic propagation models indicated in Section 2.1, and for interfaces cf. [1], Eq. (15); [18]:

$$\hat{Q}_{SB} \doteq R_0 S \hat{n} \cdot (\hat{i}_T - \hat{i}_R) \nabla_R |_{\Sigma_{S,B}} = R_0 S \hat{n} \cdot (\hat{i}_T - \hat{i}_R) s / c_0; \quad s = i\omega, \quad (2.31a)$$

for the Kirchoff approximation to the surface and bottom operator, with  $\Sigma$  = wave or bottom surface, cf. Fig. 2.1. Here  $R_0 S$  are the plane wave reflection and shadowing functions, and  $\hat{n}$  is the (inwardly drawn) normal to  $\Sigma$ . Also,  $\hat{i}_T$ ,  $\hat{i}_R$  are unit vectors in the directions of the incident and scattered wavefronts. A far-field or Fraunhofer condition is assumed. For volume inhomogeneities we have

$$Q_V = \text{Eq. (2.5b), or Eq. (2.6a); Eq. (2.9) for the PE approx. (2.8), etc.} \quad (2.31b)$$

The rôle of  $\eta^{(n)}$  in (2.13) is to generate multiple scatter components:

$$\begin{aligned}\hat{\eta}^{(2)} &= (\hat{M}_\infty Q)^{(2)} = \mathcal{L}\{(\hat{Q}_S + \hat{Q}_V + \hat{Q}_B)^2\} \\ &= \mathcal{L}\{\hat{Q}_S^{(2)} + \hat{Q}_V^{(2)} + \dots \hat{Q}_S \hat{Q}_V + \hat{Q}_V \hat{Q}_S + \dots\}\end{aligned}\quad (2.32)$$

shows the various second-order multiple scatter contributions among the various types of inhomogeneity.\* In most underwater propagation problems inter-modal scattering can be neglected, e.g., terms in  $\hat{Q}_S \hat{Q}_V$ , etc. are ignorable vis-à-vis the intra-modal contributions  $\hat{Q}_S^{(2)}$ ,  $\hat{Q}_V^{(2)}$ , which condition can considerably simplify the subsequent calculations. In any case, the structure (2.30), or "M-form," appearing in the FRO,  $\hat{\eta}$ , provides a useful "bookkeeping" of the various possible interactions.

With inhomogeneous ( $\hat{Q} \neq 0$ ) media, exact conventional techniques fail, largely because the medium is not reciprocal [cf. (iii), Sec. 2.2] and there is no general way of applying and evaluating the initial conditions over the various volume integrals which appear in the development of the Generalized Huygens Principle (GHP) [20] when  $\hat{Q} \neq 0$ . [For examples of the GHP see Sec. 7.3, [20], and pp. 512, 513, [28].] Even in the simplest cases, which are bounded homogeneous media—the boundary ( $\Sigma$ ) being the inhomogeneity here—the usefulness of the results is severely limited by the difficulty in obtaining the corresponding Green's functions,  $g_\Sigma$ , except for boundaries compatible with separable coördinate systems (for which complete sets of eigenfunctions can be obtained). A second difficulty is that the resulting GHP is basically an integral equation in the desired scattered field (i.e., scattered by the boundary surface  $\Sigma$ ),  $\alpha$ , unless it makes physical sense to specify the field *a priori* on  $\Sigma$ , an unlikely situation in most applications. A third difficulty is simply the fact that these simple cases are not the ones of principal interest. Finally, a fourth complication is that  $\hat{Q}$  is often an *integral operator*, e.g.,

$$\hat{Q}(\mathbf{R}, t | \mathbf{R}', t') = \int dt' \int Q(\mathbf{R}, t | \mathbf{R}', t') ( \ )_{\mathbf{R}', t'} d\mathbf{R}' , \quad (2.32a)$$

cf. (2.15) for  $\hat{M}_\infty$ , for example, formally, expressing the physical fact that the effects of the inhomogeneities may not be local in their interactions.

Another important reason why conventional techniques fail in the treatment of inhomogeneous media is the fact that these media are space-time variable in their inhomogeneities, e.g.,  $\hat{Q} = \hat{Q}(\mathbf{R}, t | \dots)$ , cf. (2.5), (2.6). Such media do not generally support space- and/or time-harmonic solutions, exceptions being  $\hat{Q}(\mathbf{R} | \dots)$ , which permits time-harmonic solutions, and

\* Of course, one has an appropriate  $\hat{M}_\infty$  preceding each  $\hat{Q}$ .

$\hat{Q}(t | \dots)$ , which allows space-harmonic solutions. Even the standard perturbational and variational techniques of "classical" approaches (Chapter 9, [20]) are only applicable in the case  $\hat{Q}(R | \dots)$ , when  $\hat{Q}$  is deterministic, which, of course, is often not the physical problem in ocean and atmospheric media, whose local and distributed properties are explicitly space- and time-dependent. Moreover, even these methods break down when the medium is random (i.e.,  $\hat{Q}(R | \dots)$  is stochastic). In fact, all the usual deterministic methods become nugatory when the medium, and its boundaries, are random and moving.

Even though exact analytical and standard (i.e., nonrandom) perturbational techniques fail, various useful *approximate* methods are available. The best-known of these is *ray-tracing* (a comparatively high-frequency technique [21], [22]; [29], Parts III, IV), and *modal analysis* (a comparatively low-frequency one [21]). An important recent extension of these ideas, combined with path-integral methods and super-eikonal procedures, has been developed and applied to the study of sound speed fluctuations in nonisotropic oceans by Flatté et al. [22]. All these methods are, of course, necessarily approximate and, in fact, skillful approximation is the successful heart of these approaches. In our present approach to scattering problems we seek to preserve the *exact* formal solutions in a canonical development, reserving approximations to the last possible moment. This has the conceptual advantage of explicitly identifying the disposable portions of the general result, in the contest of the particular problem ultimately to be studied. Approximations are inevitable: we attempt to postpone them as long as possible. Accordingly, in this spirit, we seek formulations which may lead to manageable computational (and occasionally analytic) solutions of (2.2), (2.4), as well as using older methods.

## 2.5 Statistical Solutions: Dyson and Bethe-Salpeter Equations

In view of the statistical character of the scattering mechanisms in most cases of physical interest, as already noted above at the beginning of Sec. 2 and in Sec. 2.1,  $\hat{\eta}$ , (2.12), is a *stochastic operator*. Thus, the "solutions" of the Langevin equation (2.4), as mentioned above, are the various *moments* of the total field  $\alpha$ , viz.

$$\langle \alpha \rangle = \alpha_H + \langle \sum_{n=1} \hat{\eta}^{(n)} \rangle \alpha_H, \quad (2.33)$$

etc. for  $\langle \alpha_1 \alpha_2 \rangle, \dots$ , with  $(\hat{M} \rightarrow (\hat{M}_\infty$  now, cf. (2.14a). Thus, to get the first moment of  $\alpha$  *all*  $(n \geq 1)$ -order moments of the FRO are required. Similarly, all  $(n, n' \geq 1)$ -moments of  $\langle \eta^{(n)} \eta^{(n')} \rangle$  are needed for  $\langle \alpha_1 \alpha_2 \rangle$ , etc. This is clearly very cumbersome and also presents questions of convergence-in-probability (CIP), e.g.,  $\|\hat{\eta}\| < 1 \rightarrow \langle \|\hat{\eta}\| \rangle, \dots \langle \|\hat{\eta}^{(n)}\| \rangle, \dots < 1(?)$ .

A way around these difficulties is provided, however, by introducing an equivalent *deterministic* relation, obtained from

$$\langle \hat{Q} \alpha \rangle \equiv \hat{Q}_1^{(d)} \langle \alpha \rangle; \therefore \hat{\eta}_1^{(d)} \equiv \hat{M}_\infty \hat{Q}_1^{(d)}. \quad (2.34)$$

Rewriting (2.12) as  $(\hat{1} - \hat{\eta})\alpha = \alpha_H$  and averaging, using (2.34), then gives the (deterministic) Dyson equation

$$\langle \alpha \rangle = (\hat{1} - \hat{\eta}^{(d)})^{-1} \alpha_H = \alpha_H + \sum_{n=1} \hat{\eta}^{(d)(n)} \alpha_H, \quad (2.35)$$

where now  $\hat{\eta}^{(d)}$  is the Equivalent Deterministic Field Renormalization Operator (EDFRO).

The evaluation of the *nonrandom* equivalent inhomogeneous operator  $\hat{Q}_1^{(d)}$  proceeds from the relation

$$\hat{Q}_1^{(d)} \left\langle \frac{\hat{1}}{(\hat{1} - \hat{\eta}_\infty)} \right\rangle \alpha_H = \left\langle \frac{\hat{Q}}{(\hat{1} - \hat{\eta}_\infty)} \right\rangle \alpha_H \quad (2.36)$$

obtained from (2.12) averaged and (2.35). Expanding  $\hat{Q}_1^{(d)}$  by

$$\hat{Q}_1^{(d)} = \sum_{m=0} \hat{A}_m^{(1)}(\mathbf{R}, t | \mathbf{R}', t') \equiv \iint Q_1^{(d)}(\mathbf{R}, t | \mathbf{R}', t') (\cdot)_{\mathbf{R}', t'} d\mathbf{R}' dt' \quad (2.37a)$$

and applying (2.37a) to (2.36), with the requirement that each term in the resulting PTSS of both sides of (2.36) be of the same operator order, give

$$\hat{A}_m^{(1)} = \langle \hat{Q} (\hat{M}_\infty \hat{Q})^{(m)} \rangle - \sum_{j=1}^m \hat{A}_{m-j}^{(1)} \langle (\hat{M}_\infty \hat{Q})^{(j)} \rangle, \quad m \geq 1. \quad (2.37b)$$

Thus,  $\hat{Q}_1^{(d)}$  is always an *integral operator*, cf. (2.37a). When  $\hat{Q}$  is purely a *fluctuation operator*, e.g.,  $\langle \hat{Q} \rangle = 0$ , which often occurs in volume scattering when boundary effects can be ignored, usually for geometrical reasons, (2.37b) simplifies considerably. Thus, for example, we find that then

$$\hat{A}_0^{(1)} = 0; \quad \hat{A}_1^{(1)} = \langle \hat{Q} \hat{M}_\infty \hat{Q} \rangle; \quad \hat{A}_1^{(2)} = \langle \hat{Q} \hat{M}_\infty^{(2)} \hat{Q}^{(2)} \rangle; \quad \dots \quad (2.37c)$$

The extension to the second-order cases is made in a similar way ([12], Sec. 4.2). For the second-order moment  $\langle \alpha_1 \alpha_2 \rangle$ , which is part of the general statistical solution to the generic Langevin Equation (2.4), we get

$$\langle \alpha_1 \alpha_2 \rangle = (\hat{1} - \hat{\eta}_{12,\infty}^{(d)})^{-1} (\hat{1} - \hat{\eta}_{1,\infty}^{(d)} \hat{\eta}_{2,\infty}^{(d)}) \langle \alpha_1 \rangle \langle \alpha_2 \rangle, \quad (2.38)$$

where  $\hat{\eta}_{1,\infty}^{(d)} = \hat{M}_{1,\infty} \hat{Q}_1$ , etc., and

$$\hat{\eta}_{12,\infty}^{(d)} \equiv \hat{M}_{1,\infty} \hat{M}_{2,\infty} \hat{Q}_{12}^{(d)} \quad (2.38a)$$

and  $\langle \alpha_1 \rangle = \langle \alpha(r_1, t_1) \rangle$ , etc. Here  $\hat{\eta}_{12,\infty}^{(d)}$  is the second-order EDFRO, cf. (2.35) et seq., and  $\hat{Q}_{12}^{(d)}$  may be determined by an extension of the approach for  $\hat{Q}_1^{(d)}$  above (2.36) et seq. It is found ([12], Sec. 4.2) that in the frequent cases where  $\langle \hat{Q} \rangle = 0$ ,

$$\hat{Q}_{12}^{(d)} = [\langle \hat{Q}_1 \hat{Q}_2 \rangle + \hat{Q}_1^{(d)} \hat{Q}_2^{(d)}] + \langle O(\hat{Q}^{(4)}) \rangle. \quad (2.38b)$$

Writing, cf. (2.37a),

$$\hat{Q}_{12}^{(d)} = \sum_{m=0}^{\infty} \hat{A}_m^{(2)}(\mathbf{R}_1, t_1; \mathbf{R}_2, t_2 | \mathbf{R}_1', t_1'; \mathbf{R}_2', t_2'), \quad (2.39)$$

and using this in the analogue of (2.36), comparing terms of similar order in the resulting PTSS expansions gives finally

$$m=0: \quad \hat{A}_0^{(2)} = \langle \hat{Q}_1 \hat{Q}_2 \rangle - \langle \hat{Q}_1 \rangle \langle \hat{Q}_2 \rangle + \hat{Q}_1^{(d)} \hat{Q}_2^{(d)}; \quad (2.39a)$$

$$m=1: \quad \hat{A}_1^{(2)} = -[\langle \hat{Q}_1 \hat{Q}_2 \rangle - \langle \hat{Q}_1 \rangle \langle \hat{Q}_2 \rangle] + [\hat{M}_{1,\infty} \langle \hat{Q}_1 \rangle + \hat{M}_{2,\infty} \langle \hat{Q}_2 \rangle]; \quad (2.39b)$$

$$m=2: \quad \hat{A}_2^{(2)} = \text{etc.}, \quad (2.39c)$$

In the important cases where  $\langle \hat{Q} \rangle = 0$ , e.g.,  $\hat{Q}$  is a purely fluctuation operator as is often the case for infinite media, all the odd-order terms in (2.39) vanish, cf. (3.15).

Equation (2.38) is a form of *Bethe-Salpeter Equation*, which is the second-order generalization of the *Dyson Equation* (2.35), and like it, is now completely deterministic. Still higher-order formulations for  $\langle \alpha_1 \alpha_2 \alpha_3 \rangle$ , ...,  $\langle \alpha_1 \alpha_2 \dots \alpha_m \rangle$ , ..., may be derived in the same formal way. These, however, appear, in most instances, to be too complex to be useful.

Finally, we note again (cf. Sec. 2.2) that an important feature of the governing Langevin



equation (2.12), (2.13), and the Dyson equation (2.35), is that they also embody a *feedback representation*, as shown in Fig. 2.2. (For the Dyson equation (2.35), one replaces  $\hat{Q}$  by  $\hat{Q}_1^{(d)}$  and  $\alpha$  by  $\langle\alpha\rangle$ .) Thus, *these scattering problems may be regarded as an extension of modern control theory*, where now the (linear) ordinary differential equations of the control format are replaced by partial differential equations of propagation in linear (inhomogeneous) random media. Similarly, initial conditions of the former are replaced by both boundary and initial conditions for the latter. This suggests that concepts and methods already available from (linear) control theory can be helpful here in achieving quantitative solutions for  $\langle\alpha\rangle$ ,  $\langle\alpha_1\alpha_2\rangle$ , etc.

## 2.6 Related Approaches: The Transport Equation

Instead of working with the Dyson equation (2.35), we can achieve formal solutions of the Langevin Equation (2.12), (2.13) by considering propagation of the *field statistics* directly, using the concept above of the equivalent deterministic medium (EDM), as embodied in the operator  $\hat{Q}_1^{(d)}$ , etc., cf. (2.34). For example, since  $\hat{M}_{\infty}^{-1}\hat{\eta}_{1,\infty}^{(d)} = \hat{Q}_1^{(d)}$ , we may write (2.4), taking the average of both sides, as

$$\langle(\hat{L}^{(0)} - \hat{Q}) \alpha\rangle = \langle\alpha_H\rangle = \alpha_H, \quad (2.40a)$$

or

$$(\hat{L}^{(0)} - \hat{Q}_1^{(d)}) \langle\alpha\rangle = \alpha_H, \quad (2.40b)$$

which is called a *Transport Equation*, or here a propagation equation of the mean (total) field,  $\langle\alpha\rangle$ . From (2.37b) et seq., it is evident that (2.40b) is an integro-differential equation in  $\langle\alpha\rangle$ . Second- and higher-order generalizations, for the propagation of  $\langle\alpha_1\alpha_2\rangle$ , etc., follow in similar fashion. (For a treatment of the propagation of field statistics, see [13], [14], Chapter 14, for instance.)

## 2.7 An Exact Solution for $\alpha$ and $\langle\alpha\rangle$

Under certain conditions it is possible to obtain exact solutions for the inhomogeneous (and total) field  $\alpha_1$ ,  $\alpha$ . Physically, this can be done for infinite media where boundary interactions can be ignored, which may be geometrically possible, so that only volume effects occur. We consider the case of deterministic inhomogeneities. It is then required that the (deterministic) inhomogeneity operator  $\hat{Q} \rightarrow \hat{Q}_{\infty}$  takes the form

$$\begin{aligned} \hat{Q}(\mathbf{R}, t | \mathbf{R}', t')_{\infty} &= \int_{(\infty)} d\mathbf{R}' \int_{-\infty}^{\infty} dt' A(\mathbf{R} - \mathbf{R}', t - t') (\ )_{\mathbf{R}', t'} \\ &= \int_{[\mathbf{k}]} \frac{d\mathbf{k}}{(2\pi)^3} \int_{B\tau_1} e^{-i\mathbf{k} \cdot \mathbf{R} + s\tau} (\ )_{\mathbf{k}, s} A_0(\mathbf{k}, s) \frac{ds}{2\pi i}, \end{aligned} \quad (2.41)$$

where  $A_0(\mathbf{k}, s) = F_R^{-1} F_t\{A(\mathbf{r}, t)\}$ , and the *kernel*,  $A$ , of  $\hat{Q}$  (2.30), is *thus of convolutional type in space and time, but  $\neq a\delta(\mathbf{R}-\mathbf{R}')\delta(t-t')$* , and is accordingly *nonlocal*. The result is

$$\alpha(\mathbf{R}, t) = F_{\mathbf{k}} F_R^{-1} \{\alpha_0\} = \int_{C_k} \frac{d\mathbf{k}}{(2\pi)^3} \int_{Br_1} \frac{G_{OT}(\mathbf{k}, s) \mathcal{Y}_0(\mathbf{k}, s)_{\infty} e^{i\mathbf{k} \cdot \mathbf{R} + si}}{1 - N_0(\mathbf{k}, s)} \frac{ds}{2\pi i} \quad (2.42)$$

$$N_0 = -\mathcal{Y}_{0,\infty} A_0$$

where  $\mathcal{Y}_{0,\infty}$  is given by (2.25a,b). Here  $C_k$  is an appropriate contour in the complex  $k$ -plane to ensure that the radiation condition ("spatial causality") is obeyed [15].  $Br_1$  denotes a two-sided Laplace transform, or Bromwich contour  $(-\infty + id, \infty + id)$ ,  $d \geq 0$ , which enables us to handle transient signals and signals of finite duration ( $d > 0$ ), as well as the steady-state cases ( $d = 0$ ), which latter reduce to the temporal Fourier transform situation, cf. Sec. 2.2. The evaluation of (2.42) is now reduced to quadratures, which may usually be carried out analytically, at least in an appropriate series form.

For *unbounded random media* the same approach may be followed. We reduce the governing Langevin equation to a Dyson equation, as above, cf. (2.41), where now  $\hat{Q}_{\infty} \rightarrow \hat{Q}_{1,\infty}^{(d)}$  and  $\alpha \rightarrow \langle \alpha \rangle$ . Equation (2.42) now applies if we replace  $\alpha$  by  $\langle \alpha \rangle$ ,  $N_0(\mathbf{k}, s)$  by  $N_{0,1}^{(d)}(\mathbf{k}, s) = -\mathcal{Y}_0(\mathbf{k}, s)_{\infty} q_{0,1}^{(d)}(\mathbf{k}, s)$ , where  $q_{0,1}^{(d)}(\mathbf{k}, s) \equiv F_R^{-1} F_t\{\hat{Q}_1^{(d)}\}$ , with the kernel of  $\hat{Q}_1^{(d)}$  having the form  $q_1^{(d)}(\mathbf{R}-\mathbf{R}', t-t')$ , cf. (2.41) above. For mixed deterministic and random media, cf. (2.1), a linear combination of operators  $\hat{Q}_{\infty}$ ,  $\hat{Q}_1^{(d)}$  with the above properties may be expected.

## 2.8 The Received Field, $X(t)$

So far, we have been considering the (total) field  $\alpha(\mathbf{R}, t)$ , at some point  $P(\mathbf{R}, t)$ , cf. Fig. 2.1. For subsequent signal processing this field must be sensed by an appropriate *receiving aperture*, or array, designated by the (linear) filter operator  $\hat{R}$ , viz.

$$X = \hat{R}\alpha, \text{ or } X = \{X_1, \dots, X_J\} = \hat{R}\alpha, \quad (j = m, n); J = MN, \quad (2.43)$$

where (2.12) now represents the received wave, in continuous or discretely sampled form in space and time. *Beam-forming* is achieved by summing over the spatial inputs, e.g.,  $X = \{\sum_m X_{j=m,n}\}$ . See Section IVB of [4].

In fact, whether we are concerned with remote-sensing of the medium or detection and classification, we must inevitably include the receiving sensor ( $s$ ), embodied in  $\hat{R}$ . Accordingly, in such cases we must replace  $\alpha$ ,  $\langle \alpha \rangle$ , etc., by  $X$ ,  $\langle X \rangle$ , etc., in the above and subsequent analyses.

This is formally straightforward, but will introduce additional computational requirements. We remark that from the viewpoint of the transmitter-receiver systems of Fig. 1.1 the fields we are dealing with here are all *signal-dependent*, i.e., they are generated by a designated active source ( $S_{in}$ , Fig. 1.1) and can produce random, signal-dependent *noise* (reverberation or incoherent scatter) in the receiver. This is in contrast to *ambient noise* fields, whose mechanisms are quite independent of the designated source  $S_{in}$ . For the purpose of the present treatment we regard the always-present ambient noise as essentially negligible; but see Sec. IV, A, [4]: the effects of ambient noise sources may be formally included if we now replace the source function  $-G_T$  by  $-G_T - G_A$ , when  $G_A$  is (also) a distributed source mechanism.

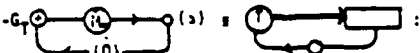
### 3. Diagram Methods and Approximations


An important aid in integrating and approximating the formal solutions of the field equations here, and in achieving numerical results eventually, are *diagram methods* ([3], [12], Part I, [16]). These enable us, along with the relevant physics, to select the dominant contributions and omit the unimportant ones, and often to choose approximations which considerably reduce the ensuing calculations. We illustrate the approach with first-order results in the case of random media.

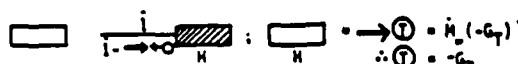
Note that for *deterministic media* these results apply as well if we drop the various averages over the Langevin ensemble, which now contains only one member field representation,  $\alpha_0$ .

#### 3.1 Basic Diagrams

We begin with the following *ensemble diagrams*, for the ensemble FOR, FOS, PTSS, etc., and FD (Feynman diagram) equivalents for the field ensemble  $\{\alpha\}$  at any allowed point  $P(R,t)$ :

FOR:  cf. Fig. 2.1 (3.1a)

FD:  Eqs. (2.10, 2.12) (3.1b)

FOS:  Eq. (2.12) (3.1c)

PTSS:  (3.1d)

Here we have  $\rightarrow (\equiv \hat{M}_\infty)$  representing the *feedforward* operator, while  $\leftarrow \circ (\equiv \hat{Q})$  denotes the ensemble *feedback* or random scattering operator,  $\hat{Q}$ . The ensemble Feynman diagram equivalent (FD) of the FOR, (3.1a), is precisely (3.1b), while (3.1c) gives the corresponding ensemble FOS, and (3.1d) the PTSS, which is readily obtained by iterating the FD, (3.1b), or as the unaveraged

form of (2.33). The (deterministic) first-order Dyson equation, Eq. (2.35) is now easily written:

*First-order Dyson Equation:*

$$\left. \begin{aligned} \Leftrightarrow &= \text{[diagram: open square with diagonal lines]} \cdot \text{[diagram: line with arrow and dot]} \cdot \Leftrightarrow \\ \langle \alpha \rangle &= \alpha_H + \hat{M}_\infty Q_1^{(d)} \langle \alpha \rangle, \text{ Eq. (4.4a),} \end{aligned} \right\} \quad (3.2)$$

where now we denote the average by  $\langle \rangle$ , applied to the corresponding ensemble symbol. Our general diagram conventions are to represent ensemble quantities as "open" forms, e.g.,  $\square$ ,  $\leftarrow \circ$ ,  $\circ$ , etc., and average and otherwise deterministic quantities by solid forms, e.g.,  $\leftarrow \bullet$ ,  $\bullet$ ,  $\bullet$ , with field averages denoted by brackets,  $\langle \rangle$ , e.g.,  $\langle \Leftrightarrow \rangle = \langle \alpha \rangle$ , etc. The aim, of course, is consistency of notation and simplicity with a minimal evolution of complexity.

Diagrams may be manipulated in the same fashion as are operator equations [cf. (2.35), etc.]: one observes the same positioning rules and conditions of inversion [cf. (2.13)], e.g., for multiplication and "division." Addition and subtraction are also directly equivalent to the addition and subtraction of operators and operator derived (algebraic) quantities, as indicated in the examples below. Finally, *transforms of diagrams are the corresponding diagrams of the transforms*. This permits an explicit diagrammatic representation of the various wave number-frequency (WNF) spectra of the scattered field, particularly the amplitude and intensity spectra in operator form.

Accordingly, the corresponding diagrams for the equivalent medium [cf. Sec. 2.5] become [cf. (3.1)]:

*Equiv. Med. FOR:*  
(2.35)

$$\text{[diagram: circle with T]} \rightarrow \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: open square with diagonal lines]} \cdot \text{cf. (2.35)}; \quad (3.3a)$$

*Equiv. Med. FOS:*  
(2.35)

$$\begin{aligned} \Leftrightarrow &= \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: open square with diagonal lines]} \cdot \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: circle with T]} \\ &= \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: open square with diagonal lines]} \cdot \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: circle with T]} \cdot \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: open square with diagonal lines]} \cdot \text{[diagram: line with arrow and dot]} \cdot \text{[diagram: circle with T]} \end{aligned} \quad (3.3b)$$

*Equiv. Med. FD:*

*First-Order Dyson Equations:*  
(2.35)

$$\Leftrightarrow = \text{[diagram: open square with diagonal lines]} \cdot \text{[diagram: line with arrow and dot]} \cdot \Leftrightarrow; \quad (3.3c)$$



remains. Let us examine, for example, the first-order Dyson equation (2.35) for the mean field  $\langle \alpha \rangle$  and postulate a first-order independent structure for  $\hat{Q}$ :

*I. First-Order Independence:*

$$\boxed{\therefore \left\langle \prod_{j=1}^n \hat{Q}_j \right\rangle = \prod_{j=1}^n \langle \hat{Q}_j \rangle} \quad \therefore = \bullet \dots \bullet_n, \quad (3.5)$$

and from (3.5) in (2.37a,b) and then in (2.35) we see at once that the  $ED_1SO$ ,  $\hat{Q}_1^{(d)}$ , is directly

$$\boxed{\hat{Q}_1^{(d)}|_{\text{indep.}} = \hat{A}_0^{(1)} = \langle \hat{Q} \rangle = \bullet; \quad \hat{A}_m^{(1)} = 0, \quad m \geq 1; \quad \therefore \hat{\eta}_{1,\infty}^{(d)} \equiv \hat{M}_\infty \langle \hat{Q} \rangle,} \quad (3.6)$$

where  $\hat{Q}_1^{(d)}$  reduces to a single term, so that (2.35) becomes at once

$$\langle \alpha \rangle = \alpha_H + \hat{M}_\infty \langle \hat{Q} \rangle \quad \langle \alpha \rangle = (\hat{1} - \hat{M}_\infty \langle \hat{Q} \rangle)^{-1} \alpha_H \quad (3.7)$$

with the following equivalent (deterministic) diagrams [cf. (3.2), (3.3)]:

$$\longleftrightarrow \bullet \cdot \frac{i}{i \rightarrow \bullet} \boxed{H} \bullet \cdot \frac{i}{i \rightarrow \bullet} \boxed{H} \bullet \cdot [i \rightarrow \bullet \dots \rightarrow \bullet^n \rightarrow \bullet] \boxed{H} \bullet. \quad (3.7a)$$

Thus, in the case of purely volume scatter ( $\langle \hat{Q} \rangle = 0$ ),  $\hat{Q}_1^{(d)} = 0$ , and  $\therefore \langle \alpha \rangle = \alpha_H$ , here, which clearly shows that the postulate (3.5) is much too restrictive to provide meaningful results in most cases.

In a similar way, we may employ a more structured, second-order assumption on the statistical character of  $\hat{Q}$ . This is the second-order "independent" or (generalized) *Bourret* or *Bi-local approximation*, defined by

## II. Second-Order Independence

$$\begin{aligned}
 \left\langle \prod_j^n \hat{Q}_j \right\rangle &= \prod_{j=1}^{n/2} \langle \hat{Q}_j^{(2)} \rangle \quad ; n = \text{even} & := \text{---} \text{---} \dots \text{---} \text{---}_{(n)} . & (3.8a) \\
 &= \prod_i^{(n-1)/2} \langle \hat{Q}_i^{(2)} \rangle \langle \hat{Q} \rangle \quad ; n = \text{odd} & := \text{---} \text{---} \dots \text{---} \text{---}_{(n)} \bullet & (3.8b)
 \end{aligned}$$

$(\hat{Q}_{i=0} \equiv \hat{1}) .$

For the odd-order case we can also set, alternatively,

$$\left\langle \prod_j^n \hat{Q}_j \right\rangle = \langle \hat{Q} \rangle \prod_i^{(n-1)/2} \langle \hat{Q}_i^{(2)} \rangle ; n = \text{odd} : = \bullet \text{---} \text{---} \dots \text{---} \text{---}_{(n)} . \quad (3.8c)$$

Consequently, the ED<sub>1</sub>SO,  $\hat{Q}_1^{(d)}$ , (2.37), (2.37a,b), becomes here

$$A_0^{(1)} + \leftarrow A_1^{(1)} \rightarrow - \leftarrow A_2^{(1)} \rightarrow + \dots :$$

$$\hat{Q}_1^{(d)}|_B = \langle \hat{Q} \rangle + [ \langle \hat{Q} \hat{M}_\infty \hat{Q} \rangle - \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle ] - [ \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle \langle \hat{Q} \hat{M}_\infty \hat{Q} \rangle - \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle \langle \hat{Q} \rangle ] + \dots \quad (3.9a)$$

or

$$\hat{Q}_1^{(d)}|_B = \langle \hat{Q} \rangle + [ \langle \hat{Q} \hat{M}_\infty \hat{Q} \rangle - \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle ] - [ \langle \hat{Q} \hat{M}_\infty \hat{Q} \rangle \langle \hat{M}_\infty \rangle \langle \hat{Q} \rangle - \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle \langle \hat{Q} \rangle \langle \hat{M}_\infty \rangle \langle \hat{Q} \rangle ] + \dots \quad (3.9b)$$

In diagram form these are:

$$q_1^{(d)}|_B = \text{---} \text{---}_{d|B} + \sum_{n=0}^{\infty} \left[ \text{---} \text{---}_{n=0} \right] + \sum_{n=1}^{\infty} \left[ \text{---} \text{---}_{n=1} \right] + \sum_{n=2}^{\infty} \left[ \text{---} \text{---}_{n=2} \right] + \dots \quad (3.9c)$$

Now, unlike the purely independent case (3.5), (3.6), ... the series for  $\hat{Q}_1^{(d)}$  does not terminate, so that in this second-order situation we are generally forced to truncate the series to obtain manageable approximations.

Note from (2.37b) that when  $\langle \hat{Q} \rangle = 0$ , which represents purely volume scatter effects





### I. Taylor Series Approximations:

Although the exact solution  $\langle \alpha \rangle$  of, say, the first-order Dyson equation (2.35), (3.2), requires an infinite PTSS, cf. (2.25), we can reduce the evaluation of  $\langle \alpha \rangle$  to a purely algebraic solution by means of a Taylor's series expansion with truncation. Thus, if we expand  $\langle \alpha \rangle$ :

$$\langle \alpha(\mathbf{R}', t') \rangle = \langle \alpha(\mathbf{R}, t) \rangle + (\mathbf{R}' - \mathbf{R}) \cdot \nabla_{\mathbf{R}} \langle \alpha(\mathbf{R}, t) \rangle + (t' - t) \frac{\partial}{\partial t} \langle \alpha(\mathbf{R}, t) \rangle + \dots, \quad (3.12)$$

and keep only the leading term, we have directly the first-order approximate form

$$[\hat{M}_{\infty} \hat{Q}_1^{(d)} \langle \alpha \rangle] \doteq \langle \alpha(\mathbf{R}, t) \rangle \hat{M}_{\infty} \hat{Q}_1^{(d)} 1 \quad (3.13a)$$

where  $\hat{M}_{\infty} \hat{Q}_1^{(d)} 1$  is simply an (analytic) function of  $(\mathbf{R}, t)$ , viz.:

$$\hat{n}_1^{(d)} 1 = \hat{M}_{\infty} \hat{Q}_1^{(d)} 1 = \int M_{\infty}(\mathbf{R}, t | \mathbf{R}', t') d\mathbf{R}' dt' \int \hat{Q}_1^{(d)}(\mathbf{R}', t' | \mathbf{R}'', t'') 1 d\mathbf{R}'' dt'' \equiv n_1^{(d)}(\mathbf{R}, t). \quad (3.13b)$$

Applying (3.13a,b) to (2.35) gives the approximate *analytic* result

$$\langle \alpha^{(1)}(\mathbf{R}, t) \rangle \doteq \frac{\alpha_H(\mathbf{R}, t)}{1 - n_1^{(d)}(\mathbf{R}, t)}, \quad (3.14)$$

where the exact or various approximate expressions for the equivalent deterministic medium operator  $\hat{Q}_1^{(d)}$  may be employed, cf. ((2.37a,b), (3.6), (3.10)). Thus, for the fully independent (I) and bi-local approximations (II),  $\langle \hat{Q} \rangle = 0$ , we have specifically (and exactly) here:

$$n_{1\text{-ind}}^{(d)} = \hat{M}_{\infty} \langle \hat{Q} \rangle 1; \quad n_{1\text{-ind}}^{(d)} = \langle \hat{Q} \hat{M}_{\infty} \hat{Q} \rangle 1, \quad \langle \hat{Q} \rangle = 0. \quad (3.15)$$

Clearly, there may be some points (foci) or lines (caustics) in space where  $\langle \alpha^{(1)} \rangle \rightarrow \infty$ , when the denominator of (3.14) vanishes. The reality of these singularities depends on how well (3.14) approximates  $\langle \alpha \rangle$  itself: the true foci, etc. may not be infinite, but may be located close to the singularities of the approximation. Thus, (3.14) may serve as a guide as to potentially real foci, etc.

Finally, the error in using (3.14), say, is generally difficult to assess, because the true

of  $\langle \alpha \rangle$  is not usually available. However, in the cases where the conditions for (2.41) are obeyed we can use the exact result (2.42) to determine the error vis-à-vis using (3.14) for  $\langle \alpha \rangle$ .

## II. Born Approximations:

Unlike the above procedures A, B, which essentially approximate the "mass operator,"  $Q^{(d)}$ , with an infinite or truncated series, cf. (3.9) or (3.10), we may truncate the PTSS [(2.13), (3.3d), etc.] directly. The resulting finite series is called a *Born approximation series*, whose order depends on the stage at which truncation is applied. Thus, for the first-order Dyson equation (3.3c) for the mean field  $\langle \alpha \rangle$  we can construct the following hierarchy of approximations and associated diagrams:

(PTSS)<sub>n</sub>:

associated diagrams:

$$n=0: \quad \longleftrightarrow \cdot \longrightarrow \textcircled{\gamma} = \text{shaded box with } \gamma \text{ and } \textcircled{\gamma}_H; \quad (PTSS)_n; \quad (FOS)_0; \quad (3.16a)$$

$$n=1: \quad \longleftrightarrow : [1 \rightarrow] \quad \boxed{H} : (FOS)_1 : \text{...} \quad (3.16b)$$

*first Born approximation*

$$n=2: \left\{ \begin{array}{l} \text{second Born approximation} \\ \text{etc.} \end{array} \right. \quad \begin{array}{l} \longleftrightarrow \doteq [1 \rightarrow \bullet \xrightarrow{2} \text{diagram}] \boxed{\text{H}}; (\text{FOS})_2; \\ \langle \alpha \rangle \doteq \sum_{n=0}^{\infty} \langle M_n \hat{O}^{(n)} \rangle \alpha_H; \\ \text{etc.} \end{array} \quad \begin{array}{l} (3.16c) \\ \text{etc. } (n \geq 3). \end{array}$$

The  $n^{\text{th}}$  order FOR is simply

$(FOR)_n$ :  
 $n^{\text{th}}$ -order Born approximation

$\Leftrightarrow (FOR)_n = \sum_{n=0}^{\infty} \langle (i_0^0)^{(n)} \rangle_H$

$(3.16d)$

Unlike the approaches above which use modifications of the "mass operator,"  $Q^{(d)}$ , etc., but where the resulting PTSS remain infinite, or where equivalently, the corresponding FOR and FOS [cf. (3.11)] contain closed feedback loops, all Born approximations contain only feed-forward loops, as indicated in (3.16d). This is the immediate consequence, of course, of the truncation of the direct PTSS (3.3d).

**Examples: Ocean Volume and Surface Channels: The Received Field X**

As examples, we noted that both the important cases of weak volume scatter in the ocean and ocean surface scatter are well approximated by at most the scattering element interacting with the homogeneous field  $\alpha_H$ , the former because multiple scatter effects are usually quite ignorable, the latter from the physical geometry of the wave surface, which likewise discourages multiple scatter except within a typical wave crest-to-crest domain (except possibly at small grazing angles).



$$\hat{Q}^{(0)} \equiv \langle \hat{Q} \rangle_R = 0, \quad \therefore \langle \hat{Q}^{(0)} \rangle_S = \langle \hat{Q} \rangle = \bullet = \langle O \rangle_R$$

$$\text{---} \equiv \langle \rangle_{S:\text{space av. } \times \theta}$$

$$\begin{array}{c} \bullet \\ \text{---} \\ \bullet \\ 1 \quad 2 \end{array} = \langle \hat{q}_1 \hat{q}_2 \rangle \text{ etc. } \text{---} = \langle \rangle = \langle \rangle_{R,S} \quad (3.19)$$

Note that the (total) average,  $\langle \rangle$ , as in [30], Appendix A.1 et seq. involves both an average over radiation events and an average over random spatial (S) and parameter values ( $\theta$ ), embodied in  $\langle \rangle_S$ , cf. (3.14) and, particularly, [30], Appendix A.2.

It is the decomposition principle, embodied in  $\hat{Q}_M$ , ( $M = S, V, B$ ), ([30], (A.2-5) et seq.), which allows us to resolve the inhomogeneity operator into sets of distinct and (statistically) independent entities as specifically exhibited in (3.18a) and (3.18b). Moreover, and most important, the entities ( $k = 0, k = 1, k \geq 2$ ) in (3.18a) and (3.18b) above and in (3.17), with the help of (3.19) have an explicit physical interpretation. Thus, the terms  $k = 0$  contain both the *coherent* and incoherent radiation contributions, from all orders ( $k \geq 1$ ) of radiation interactions, e.g., single and multiple scattering ( $k \geq 2$ ), for example. Consequently, if  $v^{(k)}$  represents the density of (illuminated)  $k$ -coupled scattering elements ( $k > 1$ ), then  $\langle v^{(k)} \rangle_R$  is the coherent radiative contribution, where  $\langle \rangle_R$  is the average over the radiation events associated with the ensemble of potential (re-)radiating sources. In a similar way

$$\Delta v^{(k)} \equiv v^{(k)} - \langle v^{(k)} \rangle_R \quad (3.20a)$$

is the *fluctuation* in the density of  $k$ -coupled radiating elements, and is always associated with incoherent radiation. Accordingly, we have

$$v^{(0)} \equiv \sum_{k=1}^{\infty} (\langle v^{(k)} \rangle_R + \Delta v^{(k)}) = \sum_{k=1}^{\infty} v^{(k)} \equiv v \equiv \langle v^{(0)} \rangle_R + \Delta v^{(0)} \quad (3.20b)$$

showing the basically coherent and incoherent elements of the scattering or source region containing these various  $k \geq 1$  types of elements. The (average) density of coherent radiators is  $\langle v^{(0)} \rangle_R = \sum \langle v^{(k)} \rangle_R$ , since  $\langle \Delta v^{(k)} \rangle_R = 0$ . The number of "radiation events" occurring in a small region  $d\Lambda$  of the illuminated or emitting domain  $\Lambda$  is  $dN$ , so that  $v = dN/d\Lambda = v^{(0)}$ . A taxonomy and interpretation for the  $dN$ , similar to (3.20a), (3.20b), can be constructed: one now has

$$dN^{(0)} \equiv \sum_{k=1}^{\infty} (\langle dN^{(k)} \rangle_R + dn^{(k)}) = \sum_{k=1}^{\infty} dN^{(k)}. \quad (3.20c)$$

The relations (3.21) et seq. obviously apply if one replaces  $v$  etc. by  $dN$ .

Since the medium in question is linear, the scattering or inhomogeneity operator  $\hat{Q}$  is a linear functional of the  $v(k)$ , i.e., of  $v^{(0)}$ , e.g.,  $\hat{Q} = \mathcal{L}(v^{(0)})$ , thus containing all types of radiation interaction effects. Moments of  $v^{(0)}$ , or more generally, of  $\hat{Q}_M$ , which appear in (3.17) and (3.18), above, are readily indicated: we have

$$\langle \hat{Q} \rangle = \mathcal{L}\{\langle v^{(0)} \rangle\}$$

where

$$\langle v^{(0)} \rangle = \langle \langle v^{(0)} \rangle_R \rangle_S. \quad (3.21)$$

This is different from zero, in scattering, if specular reflection geometry (both on a surface and in a volume) is available. The second-order moments are instructive:

$$\langle \hat{Q}_1 \hat{Q}_2 \rangle = \mathcal{L}\{\langle v_1^{(0)} v_2^{(0)} \rangle\} \quad (3.21a)$$

where now

$$\langle v_1^{(0)} v_2^{(0)} \rangle = \langle \langle \Delta v_1^{(0)} \Delta v_2^{(0)} \rangle_R \rangle_S + \langle \langle v_1^{(0)} \rangle_R \langle v_2^{(0)} \rangle_R \rangle_S. \quad (3.21b)$$

with

$$\Delta v^{(0)} \equiv \sum_{k=1} \Delta v(k).$$

Equation (3.21b) contains both incoherent ( $\sim \Delta v^{(0)}$ ) and coherent terms ( $\sim \langle \Delta v^{(0)} \rangle_R$ ), of all orders ( $k \geq 1$ ) of coupled scattering or radiating elements. The associated covariance of  $\hat{Q}$  is

$$K_{\hat{Q}} = \mathcal{L}\{\langle v_1^{(0)} v_2^{(0)} \rangle - \langle v_1^{(0)} \rangle \langle v_2^{(0)} \rangle\} \quad (3.21c)$$

which embodies wholly incoherent radiation.

As in all these approximate situations, the evaluation of error remains a major, very difficult problem, because the exact results are generally unknown. We must rely, instead, on our physical intuition, aided by the (essentially) local physics governing the inhomogeneity operator  $\hat{Q}$  in question. This is one reason why the physical "anatomization" of the so-far canonical  $\hat{Q}$  is critically important in specific cases.

### 3.3 An Estimation Procedure for the Mean Operator

When the elements  $(-G_T, \hat{M}_{\infty})$  of the "input-output" structure of Fig. 2.2 are available, estimates of the "mass operator"  $\hat{Q}_1^{(d)}$  may be made to any degree of accuracy from the empirical or a priori mean field  $\langle \alpha \rangle$ , in a controlled way, in principle, with determinable error. This is a form of "system identification" problem, typical of control theory [24]. Here, in essence, one

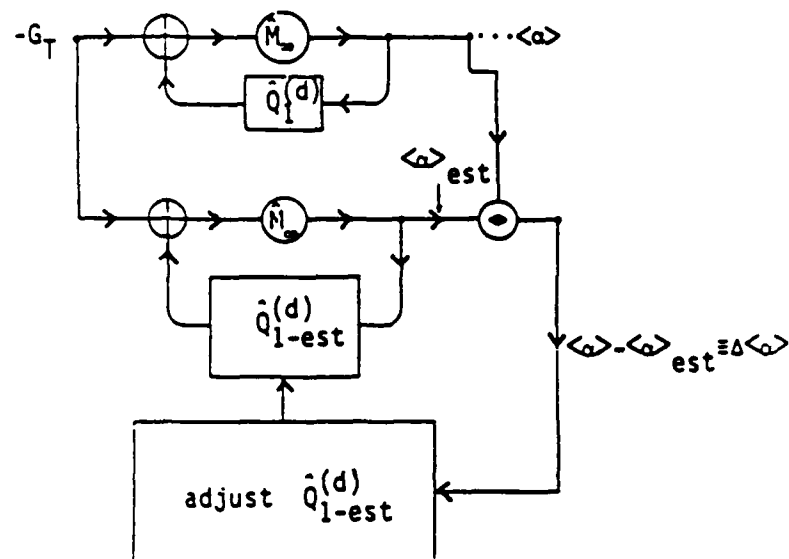


Fig. 3.1 Feedback-operational method for obtaining the (first-order) equivalent medium (integral) operator  $\hat{Q}_1^{(d)}$ .

introduces a "black-box" or system with a controllable input, observes the resulting output(s), and attempts to infer the operations of the system which relates the two. A key feature here is that the system in question is known to be linear, so that unique relations are established.

For (2.34) to be a *physically* (vis-à-vis mathematically) useful device, we must be able to indicate a physical procedure for determining  $\hat{Q}_1^{(d)}$ . This may be done according to the scheme shown here in Fig. 3.1. This scheme produces a converging series of estimates,  $\hat{Q}_{1-est}^{(d)}$ , for  $\hat{Q}_1^{(d)}$ , by iteration, when  $[\langle \alpha \rangle, -G_T]$  are provided *experimentally*, and when  $\hat{M}_\infty$  is either empirically or analytically given. The basic approach is conceptually quite simple: with a starting estimate  $\hat{Q}_{est-1}^{(d)}$  of  $\hat{Q}_1^{(d)}$ , one runs through the second loop, using the (experimentally) observed  $\langle \alpha \rangle$ , the given source,  $-G_T$ , and the known global descriptions of the homogeneous component of the medium ( $\hat{M}_\infty$  here, cf. Sec. 2.2), to get an  $\langle \alpha \rangle_{est}$ . This is then subtracted from the observed  $\langle \alpha \rangle$  from the first-loop, which in turn leads to an adjustment of  $\hat{Q}_{1-est}^{(d)}$ , a second comparison, with a further reduction in the error  $\Delta \langle \alpha \rangle = \langle \alpha \rangle - \langle \alpha \rangle_{est}$  and  $\Delta \hat{Q}_1^{(d)} = \hat{Q}_1^{(d)} - \hat{Q}_{1-est}^{(d)}$ . Various optimum and suboptimum schemes from control theory (e.g., Wiener filtering, gradient-climbing, etc., now, however, extended to *four* dimensions) may be used to drive the errors  $\Delta \langle \alpha \rangle$ ,  $\Delta \hat{Q}_1^{(d)}$  essentially to zero, so that  $\hat{Q}_{1-est}^{(d)} \rightarrow \hat{Q}_1^{(d)}$ . This technique may also suggest acceptable approximations in experimental situations. In fact, approximating  $\hat{Q}_1^{(d)}$  here is analogous to choosing some approximation to  $\hat{Q}_1^{(d)}$ , (2.37), like  $\hat{A}_0$ , or  $\hat{A}_1$ , cf. (2.37 a,b,c) et seq.

In all cases the particular physics of the problem will dictate the procedural details, the approximations (usually required), and the class of "hardware" to be employed, e.g., minicomputer, minisupercomputer, or supercomputer. Some form of the latter appears necessary

in most cases, cf. Sec. 4 ff., since these problems are generally on the scale of long-range weather prediction. In fact, these problems may be considered as a form of "underwater weather" prediction, especially when the medium (and interface) behavior is properly included. It is hoped that the preceding material may provide at least a stimulus to the much-needed and as yet nonexistent computational solutions to this important class of problems.

#### **4. Concluding Remarks: Analytic Steps to the "Interface Problem"**

As we have noted at the beginning of this paper, a principal purpose of this study is to bring the formal analytic-operational treatment to the point where the computational problems of implementing these formal results numerically can be addressed. We call this the "Interface Problem," where the interface lies between the general mathematical formulation, outlined here, and software design and hardware performance.

The various steps which can bring the analytical treatment to this interface (the dotted line) are summarized in Table 4.1.

Our philosophy here has been to start with as general a "top-down" approach as possible, including those physical features which can ultimately influence practical solutions. Among such features are beam patterns, signal waveform, and, of course, geometry, as well as the relevant structures of the medium inhomogeneities. Proceeding with particular applications, we usually find that approximations and simplifications can be made which can significantly reduce the very heavy computational burdens implied by the operational forms of the desired "solutions." The latter, of course, are both deterministic and stochastic, and a full treatment will need to include both these components. The present problems are on the scale of weather prediction problems. In fact, they are themselves models of "underwater weather." With the recent advances in computer capabilities (and reduced costs) we may expect these problems to be within range of numerical solution: The present effort has been presented, in part, to stimulate their numerical investigation, as well as the achievement of further analytic solutions.

Table 4.1

Step	Deterministic Inhomogeneities	Step	Random Inhomogeneities
1.	Obtain the PDE and b.c.'s + i.c.'s; Eq. (2.1) et seq.; = "Dynamical Equation"; all representations are equivalent here	1.	Obtain the PDE, b.c.'s + i.c.'s; Eq. (2.1) et seq., for a typical representation
2.	Obtain the infinite-medium Green's function $g_{\infty}$ , cf. (2.24), (2.26), (2.27)	1a.	Construct the Langevin Equation, Eq. (2.4) et seq.
3.	Operational Solutions: These are complete: PTSS, FOS from the FOR, cf. (2.13), Fig. 2.2., Sec. 2.3, 2.4 for $\hat{Q}$ , the inhomogeneity operator, cf. (2.5b), (2.6a). (2.9)	2.	Same
4.	Approximate $\hat{Q}$ , local and distributed. Use <i>diagram methods</i> , Sec. 3.2 [ $\hat{Q}$ is usually local, cf. (2.5b), (2.6a), (2.9)]	3.	Solutions are the <i>statistics</i> of the field $\alpha$ , e.g., $\langle \alpha \rangle$ , $\langle \alpha_1 \alpha_2 \rangle$ , etc., and pdf's $w_1(\alpha)$ , $w_2(\alpha_1, \alpha_2)$ , ...
5.	Analytic solutions (for volumes only), cf. Sec. 2.7, Eq. (2.42)	3a.	Construct <i>Dyson's equation</i> (first-order), Sec. 2.5 for Equivalent Deterministic Media (EDM), sol. $\langle \alpha \rangle$
6.	Other Approximations: Ray tracing, normal modes (time-independent) [21]; $\hat{Q}(\mathbf{R}   \dots)$ —time-harmonic solutions; $\hat{Q}(t   \dots)$ —space harmonic sol.; $\hat{Q}(\mathbf{R}, t   \dots)$ —sol. not harmonic. Medium non-reciprocal, so Generalized Huygens Principal <i>not</i> available. Path Integrals, Super-Eikonal Methods [22], [23]	3b.	Higher order: $\hat{Q}_2^{(d)}$ , for $\langle \alpha_1 \alpha_2 \rangle$ , etc. PTSS; FOS forms (2.35); Some analytic solutions, Sec. 2.7
7.	Computational Solutions: special cases only (no boundaries) [7], [10]. General software: to be estimated, approx. and exact.	4.	Approximate $\hat{Q}_1^{(d)}$ , etc., Sec. 2.5; <i>Diagram methods</i> assist; Sec. 3, Sec. 3.2; $\hat{Q}_1^{(d)}$ is non-local; all higher-order $\hat{Q}^{(d)}$ 's are also non-local
		5.	Analytic solutions (volumes only), cf. Sec. 2.7, Eq. (2.42) modified, 2nd ¶; 1st order. Higher-order by similar way, but very complicated.
		6.	Same, for (EDM), (EDM) <sub>2</sub> , via $\hat{Q}_1^{(d)}$ , etc. (See [12] for details.) Realization of diagram approximations
		7.	Computational Solutions: generally unknown. To be constructed, approx. and exact = Major Problem.



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## Glossary of Principal Symbols

$\alpha, \alpha(R,t)$	= total field, at $P(R,t)$
$\mathcal{Q}_T, \mathcal{Q}_R$	= beam patterns
$\alpha_H$	= homogeneous field
$Br_1$	= Bromwich contour, (two-sided Laplace transform)
$c_0$	= mean sound speed
$\nabla c$	= sound speed gradient
$\nabla^2$	= Laplacian (in rectangular coördinates)
$\epsilon, \epsilon(R,t)$	= (function of) index of refraction
$\hat{\eta}, \hat{\eta}^{(d)}$	= field renormalization operators (FRO), (EDFRO)
FD	= Feynman diagram
FOR	= feedback operational representation
FOS	= feedback operational solution
FRO	= Field Renormalization Operator
${}_1F_1$	= confluent hypergeometric function
$\mathcal{F}, \mathcal{F}^{-1}$	= Fourier transforms
$\hat{G}, G$	= input source operators and functions
$g_\infty$	= Green's function of an unbounded medium
$\hat{i}_x, \hat{i}_y, \hat{i}_z$	= unit vectors
$k, k$	= wave numbers
$\hat{L}^{(0)}$	= differential operator for homogeneous part of medium
$\mathcal{L}$	= linear operator, cf. Eq. (2.22)
$\hat{M}, \hat{M}_\infty$	= integral Green's function operator
$N_0, N_{01}^{(d)}$	= field renormalization functions
PTSS	= perturbation theoretical series solution
$\hat{Q}, \hat{Q}_1^{(d)}, \hat{Q}_{S,V,B}, \dots$	= inhomogeneity operators
$R$	= position vector in rectangular coördinates
$\hat{R}$	= receiving array operator
$S_{in}$	= input signal
$s$	= (complex) angular frequency
$T_M^{(N)}$	= medium operator
$X, X(t)$	= receiver array outputs to signal processor
$\mathcal{X}_{0,\infty}, \hat{\mathcal{X}}_{0,\infty}, \hat{Y}_{0,\infty}$	= Fourier and Laplace transform of $g_\infty$
$\hat{1}$	= unit operator

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